

Geotechnical Investigation Report
BIA Project N12 (12-2)(19-2)2&4
Navajo, New Mexico to N64 Junction, Arizona (near Tsaile)
Five Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek;
N614, Coyote Wash; N613, Tohdildonih Wash
BIA Order No. A13PD00246
BIA Requisition No. 0040100785
Architect – Engineer IDIQ Contract No. A12PC00121

#### Submitted to:

Bureau of Indian Affairs, Navajo Regional Office Gallup, New Mexico

# Submitted by:

AMEC Environment & Infrastructure, Inc. Phoenix, Arizona

**September 22, 2014** 

AMEC Project No. 17-2013-4030 Revision No. 1





September 22, 2014 AMEC Project No. 17-2013-4030.0001 Revision No. 1

Bureau of Indian Affairs, Navajo Regional Office Division of Acquisition PO Box 1060 301 West Hill, Room 346 Gallup, New Mexico 87305-1060

Attn: Corwyn Henry

Re: Geotechnical Investigation Report

BIA Project N12 (12-2)(19-2)2&4

Navajo, New Mexico to N64 Junction, Arizona (near Tsaile)

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Creek; N614, Coyote Wash; N613, Tohdildonih Wash

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AMEC Environment & Infrastructure, Inc. (AMEC) has revised our Preliminary Geotechnical Investigation of the subsurface conditions at five bridge sites on Bureau of Indian Affairs (BIA) Route N12 based on comments received on August 29, 2014. The bridge sites consist of bridges N505 at Tsaile Creek, N504 at Wheatfield Creek, N503 at Whiskey Creek, N614 at Coyote Wash, and N613 at Tohdildonih Wash. The bridge sites are contained between Navajo, New Mexico and N64 Junction near Tsaile, Arizona. This work was performed in general accordance with BIA Order No. A13PD00246 dated July 13, 2013. The results of our investigation along with the boring location plans and boring logs are attached.

We at AMEC are committed to providing quality engineering services combined with client satisfaction in order to achieve a continuing relationship with our clients. We appreciate the opportunity to provide these services for you. If you have any questions regarding any of the other engineering and testing services AMEC provides, please do not hesitate to contact us.

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Respectfully submitted,

AMEC Environment & Infrastructure, Inc.

MARK HARTIG Reviewed by:

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#### 1.0 PROJECT INFORMATION AND PURPOSE

Included in this report are the results of our subsurface investigation at five bridge sites along Bureau of Indian Affairs (BIA) Route N12 from Navajo, New Mexico north to N64 Junction near Tsaile, Arizona. The five bridge sites consist of bridges N505 at Tsaile Creek, N504 at Wheatfield Creek, N503 at Whiskey Creek, N614 at Coyote Wash, and N613 at Tohdildonih Wash. At the request of the BIA, our investigation was in general accordance with IDIQ Contract No. A12PC00121, Section D, Bridges and Other Major Structural Element Soils Investigations, Sampling, & Testing, along with the following exceptions:

- Per e-mail from Ms. Ella Dempsey on June 6, 2013
  - o References to "recommended structure" or "recommended replacement structure" shall be changed to say "structure to be recommended in the future".
  - Boring Plan development shall be based on existing foundation elements of the existing bridges currently in place.
  - Section D. 1. (a). (1). (C). does not apply since the approach roadway investigation will fall under the roadway portion of this RFP.
  - The Section D. 1. (a). (2). (B). reference to the prohibition of the Modified California sampler can be revised to say, "The Modified California sampler shall only be used to obtain samples but shall not be used to determine blow counts of the soil being sampled. Blow counts shall be determined by a standard, non-modified sampler."
  - A "structure specific" foundation design is not required since a specific recommended structure is not available. However, the consultant shall provided a recommended structure type (system) based on the subsurface characteristics encountered that will best support a standard highway bridge structure. The data gathered from the investigation and laboratory analyses shall be sufficient to design a foundation for a structure to be determined in the future.
- Per direction from Mr. Harold Riley on August 1, 2013, via telephone call
  - o Proposed borings at the midpoints (upstream and downstream) of the single span bridges (N503, N504, N505, and N614), and the proposed borings at each pier of Bridge N613 (4 span bridge) are not to be performed.

This report does not address any environmental issues related to the site or the project. If you have any questions concerning environmental aspects of this project please contact us and we can discuss additional services with you.

Our professional services have been performed using that degree of care and skill ordinarily exercised, under similar circumstances, by reputable geotechnical consultants practicing in this or similar localities. No other warranty, expressed or implied, is made as to the professional advice included in this report. This report has been prepared for BIA, Navajo Regional Office for the purpose of providing the information described above. This report has not been prepared for any other parties, and may not contain sufficient information for purposes of other parties. If



any of the project information described in Section 2.0 of this report has changed, we should be notified so that we may amend our recommendations, as necessary.

#### 2.0 FIELD EXPLORATION AND LABORATORY TESTING

## 2.1 Field Exploration

AMEC Environment & Infrastructure, Inc. (AMEC) advanced one boring at each end of each existing bridge abutment between the dates of September 17 and October 27, 2013. The borings were performed under the direction of Reed Seamons, AMEC field geologist. The borings were performed by Cascade Drilling with a buggy-mounted CME 85 drill rig using 203 millimeter diameter hollow stem auger (HSA) and 96mm (HQ) outside diameter rock coring. The rock coring was advanced using a HWT casing advancer and HQ-sized, wireline, diamond-bit, rock coring system. The HQ core system produces 63.5millimeter-diameter core and a 96-millimeter-diameter borehole. All borings were drilled in a vertical orientation. Per the requirements of the contract, the borings were augered to approximately 30.5 meters in depth or until bedrock was encountered. If bedrock was encountered, rock coring was performed to a depth of approximately 6 meters or greater depending on percent recovery. Standard penetration testing and open-end drive sampling were generally performed every 1.5 meters within the soil section of the borings. Below is a summary of the auger and core drilling performed at the bridge locations:

- Bridge N505: Augered to bedrock encountered at depths between 2.7 and 4.4 meters below ground surface (bgs). Cored to depths between 9.3 to 15.4 meters bgs.
- Bridge N504: Augered to depths between 28.2 to 30.5 meters bgs. No rock coring. Note: Boring N504 B-2 stopped at 28.2 meters due to auger/mechanical difficulties.
- Bridge N503: Augered to bedrock encountered at depths between 8.8 and 11.9 meters bgs. Cored to depths between 15.4 and 18.3 meters bgs.
- Bridge N614: Augered to bedrock encountered at depths between 7.6 and 11.6 meters bgs. Cored to depths between 13.7 and 17.7 meters bgs.
- Bridge N613: Augered to bedrock encountered at depths between 7.6 and 16.2 meters bgs. Cored to depths between 14.0 and 22.3 meters bgs.

Borings performed were backfilled with soil cuttings and grout in the upper 6 meters. Excess soil cuttings were spread nearby. In some locations, the borings were performed through the existing asphalt pavement. These locations were backfilled as described above; however the surfaces were patched with cold patch asphalt, tamped down with a mallet, and were left slightly mounded to allow for some settlement. Soil borings were numbered B-1 through B-4 at each bridge location, with B-1 at the northwest abutment, B-2 at the northeast abutment, B-3 at the southwest abutment, and B-4 at the southeast abutment.

The approximate locations of the soil borings are shown on Figures 1 through 6 – Project Overview and Boring Locations Map. The GPS NAD 83 – UTM Zone 12 coordinates for each location were established using a handheld survey grade GPS unit and are shown on the attached boring logs along with elevations. The soils and bedrock encountered at each location were visually classified and recorded on a field log. After completion of the laboratory tests on



the samples retrieved, the field logs were reviewed and modified where necessary to produce the final boring logs presented in Appendix A. Additionally, descriptions of the drilling techniques used, a summary of the Unified Soil Classification System (ASTM D2487) and an explanation of the terminology used in describing rock core can be found in Appendix A. Our field and final classifications were based on the Unified Soil Classification System (USCS) and AMEC guidelines.

# 2.2 Laboratory Testing

Laboratory tests were performed on the representative bulk, split spoon, and undisturbed samples obtained during our field exploration for the purpose of evaluating the pertinent engineering properties of the site soils. The following tests were performed in general accordance with the applicable American Association of State Highway and Transportation Officials (AASHTO) test methods:

- Plasticity Index (AASHTO T89, T90)
- Sieve Analysis (Gradation and Minus #200 wash) (AASHTO T11,T27)
- Direct Shear (AASHTO T236) 3-point in-situ
- Unconfined Compression of Cohesive Soil or Rock Core (AASHTO T208)
- Consolidation (AASHTO T216)

The laboratory results are summarized in Table C-1 of Appendix C and are followed by copies of the laboratory reports.

#### 2.3 Geologic Setting

The project area is located in the Colorado Plateau geologic province along the western base of the Chuska Mountains in northeastern Arizona and northwestern New Mexico. The geologic units underlying the project corridor typically consist of recent unconsolidated deposits of varying thickness underlain by Triassic-age rock formations: the Chinle and Wingate Formations (Byers 1980, O'Sullivan and Beikman 1963 and Thaden 1990).

The Chinle Formation is the geologic formation present throughout most of the corridor. It is subdivided into several Members, three of which are present along the project corridor: Red Member, Owl Rock Member, and the Petrified Forest Member. The Red Member of the Chinle Formation is present in the northernmost portion of the corridor and typically consists of dark reddish-brown bentonitic siltstone, sandstone and lime-pellet conglomerate. The Owl Rock Member of the Chinle formation is present along much of the corridor and typically consists of interbedded limestone and reddish-brown, clayey siltstone. The Petrified Forest Member of the Chinle Formation periodically occurs throughout the corridor and typically consists of blue to gray to red to white bentonitic claystone, siltstone and sandstone (Byers 1980, O'Sullivan and Beikman 1963 and Thaden 1990).

The Red Member of the Chinle Formation occurs at the bridge at Tsaile Creek (N505). In this area the Red Member typically consists of reddish-brown sandstone.



The Petrified Forest Member of the Chinle Formation is present at the bridge at Wheatfield Creek (N504). The Petrified Forest Member of the Chinle Formation typically consists of blue to gray to red to white bentonitic claystone, siltstone and sandstone.

The Petrified Forest Member of the Chinle Formation occurs in the area of the Whiskey Creek Bridge (N503). In this area the Petrified Forest Member of the Chinle Formation typically consists of reddish-brown calcareous siltstone.

The Owl Rock Member of the Chinle Formation is present at the bridge at Coyote Wash (N614). In this area the Owl Rock Member typically consists of reddish-brown to purplish siltstone and claystone.

Both the Owl Rock and Petrified Forest Members of the Chinle Formation occur in the area of the Navajo Bridge (N613) and it is difficult to tell for certain how the rock in this area is best categorized. The Chinle Formation typically consists of reddish-brown to purplish siltstone, claystone and mudstone.

# 2.4 Geotechnical Profile

#### N505 at Tsaile Creek

Native subgrade soils consisted of clayey sands and sandy clays with traces of fine gravel to depths ranging from 1.5 to 4.4 meters bgs, overlaying approximately 1 meter thick layer of clayey gravels and silty sands in Borings B-1 and B-4, respectively. Plasticities range from low to medium. The soil profiles generally ranged from firm to hard. Groundwater was not encountered. Sandstone bedrock was encountered at depths between 2.7 and 4.4 meters bgs. The sandstone was generally slightly to moderately weathered, with some unweathered sandstone encountered in Boring B-4. Boring B-2 had poor recovery of the rock core, and therefore several extra runs of core were performed for a total of approximately 11 meters. See the N505 boring logs for full descriptions of the soil and rock encountered.

# N504 at Wheatfield Creek

Native subgrade soils consisted of silty sands, silty sandy clays, sands, sandy silts, and gravelly sands to depths of approximately 10.7 to 12.5 meters bgs. These materials were overlaying clays, clayey silts, and silty clays (possibly claystones or siltstones) to the full depths of exploration, 30.5 meters bgs. Plasticity ranged from low to medium for the silty sandy clays, clayey silts, and silty clays, and was generally nonplastic for the silty sands and sands. The soil profiles generally ranged from moderately firm to hard to depths of approximately 10.7 to 12.5 meters bgs, and hard below that to the full depth of exploration. Groundwater (possibly perched on the claystone/siltstone type material) was encountered at depths ranging from 6.4 to 7.6 meters bgs in the soil borings performed. See the N504 boring logs for full descriptions of the soils encountered.



# N503 at Whiskey Creek

Native subgrade soils consisted of sandy clays and clayey sands with occasional to some gravel overlaying silty sands, sandy silts, and sandy clays with occasional fine-grained gravels. These were generally overlaying a silty gravel layer, followed by more silty sands, sands, and sandy silts with varying amounts of gravels. Plasticity ranged from low to medium for the clayey sands, sandy clays, and sandy silts, and was generally nonplastic for the silty sands, sands, and gravels. The soil profiles generally ranged from moderately firm to hard. Groundwater (possibly perched on the bedrock) was encountered at depths ranging from 4.6 to 5.6 meters bgs in the soil borings performed. Calcareous siltstone bedrock was encountered at depths between 8.8 and 11.9 meters bgs. The siltstone was generally slightly to moderately weathered, with some highly weathered siltstone encountered in Boring B-1 near 12 meters bgs. See the N503 boring logs for full descriptions of the soil and rock encountered.

# N614 at Coyote Wash

Native subgrade soils consisted of clayey sands with some to considerable gravels ranging from approximately 3 to 7.75 meters in all four borings. The clayey sands were underlain by silty sands, sandy clays, sands, and sandy silt and clay with varying amounts of gravel. Plasticity ranged from low to medium for the clayey sands, sandy clays, and sandy silt and clays, and was generally nonplastic for the silty sands and sands. The soil profiles generally ranged from moderately firm to hard, with some soft layers encountered in Boring B-1 between approximately 4.5 and 6 meters, and 9.2 and 10.7 meters. Groundwater was not encountered. Siltstone/claystone bedrock was encountered at depths between 7.6 and 11.6 meters bgs. The siltstone/clayestone was generally slightly to moderately weathered, with some highly weathered siltstone/clayestone encountered in Boring B-2 near 13 meters bgs. See the N614 boring logs for full descriptions of the soil and rock encountered.

#### N613 at Tohdildonih Wash

Native subgrade soils generally consisted of clayey sands and silty sands with varying amounts of gravel overlaying sandy clays and sandy silts. Boring B-3 encountered a 0.5 meter thick sandy gravel layer at the surface. Plasticity ranged from low to medium for the clayey sands, sandy clays, and sandy silts, and was generally nonplastic for the silty sands and gravels. The soil profiles generally ranged from very soft to hard, with blow counts as low as 2 encountered at varying depths. Groundwater (possibly perched on the bedrock) was encountered at depths ranging from 4.3 to 5.2 meters bgs in the soil borings performed. Borings B-1, B-2, and B-4 encountered siltstone bedrock at depths between 7.8 and 10.7 meters bgs. Boring B-3 encountered a calcareous mudstone bedrock at a depth of 16.2 meters bgs. The siltstone was generally slightly to moderately weathered, with some highly weathered siltstone encountered in Boring B-4 near 10.5 meters bgs. The mudstone was generally slightly to moderately weathered. See the N613 boring logs for full descriptions of the soil and rock encountered.



# 2.5 Foundation Type Recommendations

AMEC understands that the BIA plans to widen Bridge 613 at Tohdildonih Wash. The existing bridge structure and superstructure will remain and the abutments and piers will be extended laterally to provide a wider deck. The four other bridges, N505, N504, N503, and N614; are planned to be removed and replaced. There is potential that these structures will be replaced with precast concrete arch structures, such as ConSpan arch structure. AMEC reviewed preliminary details for the ConSpan arch structures and identified the following items that need to be considered further if these structures are used:

- 1. The maximum span available for a ConSpan arch structure is 48 feet. The estimated spans for these four bridges are between 80 and 100 feet resulting in the need for a two-span structure.
- 2. A two-span structure will require a pier in the middle of each wash or creek, which will impact the hydrology and the potential scour.
- 3. The current investigation only investigated the abutment locations for these structures. Additional geotechnical investigation would be required to identify the conditions at the pier locations.
- 4. The use of a ConSpan arch structure does not dictate the foundation type required. These structures only require a surface large enough to allow a keyway to be constructed where the ConSpan arch leg is placed. Either spread footings or pile/pier caps would be suitable.

The preliminary foundation type recommendations in this report were based on the soils/bedrock encountered in the test borings performed. It has been assumed that conditions between abutment borings are representative of the soil/bedrock conditions encountered in the abutment borings.

#### N505 at Tsaile Creek

Sandstone bedrock was encountered at relatively shallow depths at this location (2.7 to 4.4 meters bgs). If desired, a new bridge structure could be supported on spread footings keyed into the sandstone bedrock or by appropriately sized drilled shafts (also known as cast-in-drilled hole [CIDH] piles, caissons, and cast-in-situ piles). Drilled shafts, if used, should be socketed into the sandstone bedrock.

#### N504 at Wheatfield Creek

The varying soil profile and consistency doesn't lend itself to shallow foundations. Lightly to moderately loaded structures could be founded on spread footings below a depth of 3 meters. Moderately to heavily loaded structures should be supported by appropriately sized drilled shafts (also known as cast-in-drilled hole [CIDH] piles, caissons, and cast-in-situ piles). Groundwater was encountered at depths ranging from 6.4 to 7.6 meters bgs, and should be accounted for when planning construction of the foundations.



### N503 at Whiskey Creek

The varying soil profile and consistency doesn't lend itself to spread footing foundations without considerable mitigation of the native soils. Therefore, we recommend a new bridge structure be supported by appropriately sized drilled shafts (also known as cast-in-drilled hole [CIDH] piles, caissons, and cast-in-situ piles). Groundwater was encountered at depths ranging from 4.6 to 5.6 meters bgs, and should be accounted for when planning construction of the foundations. To increase the end bearing capacity, the drilled shafts could be socketed into the siltstone bedrock encountered between 8.8 and 11.9 meters bgs.

#### N614 at Coyote Wash

The soil profile consists of considerable soft to moderately firm zones in the upper 10 meters ruling out the use of spread footing foundations. Therefore, we recommend a new bridge structure be supported by appropriately sized drilled shafts (also known as cast-in-drilled hole [CIDH] piles, caissons, and cast-in-situ piles). To increase the end bearing capacity, the drilled shafts could be socketed into the siltstone/claystone bedrock encountered between 7.6 and 11.6 meters bgs.

#### N613 at Tohdildonih Wash

The soft to very soft soils in the upper 8 to 13 meters at the north and south abutments respectively, preclude the use of spread footing foundations. Furthermore, the use of spread footing foundations would result in increased differential settlement between the existing structure and the proposed widened structure. Therefore, AMEC recommends that the widened portion of the bridge be supported on drilled shafts (also known as cast-in-drilled hole [CIDH] piles, caissons, and cast-in-situ piles). The use of drilled shafts will allow adequate capacity to be obtained while reducing the potential differential settlement between the existing structure and the proposed widened structure. There is potential that the drilled shafts will need to be socketed into the siltstone bedrock encountered at approximately 8 to 16.2 meters bgs at the north and south abutments, respectively. Groundwater was encountered at depths ranging from 4.3 to 5.2 meters bgs, and should be accounted for when planning construction of the foundations.

#### 2.6 Preliminary Foundation Design Recommendations

At the request of the BIA, AMEC has developed preliminary recommendations for unit side resistance and unit end bearing resistance for drilled shafts socketed into rock for all bridge locations. In addition, preliminary unit side resistance and unit end bearing resistance for driven steel H piles has been developed for bridge N613 since this bridge is currently founded on driven steel H piles. The recommendations are preliminary due to no borings being done at the bridge pier locations and due to the unknown scour depth at each bridge location. This additional information would be required prior to finalization of these recommendations.



# **Preliminary Nominal Resistance**

	Drilled Shaft		H-Pile	
Bridge	Unit Side Resistance, kPa	Unit End Bearing Resistance, kPa	Unit Side Resistance, kPa	Unit End Bearing Resistance, kPa
N505	500	1,300		
N504	80	150		
N503	370	510		
N614	280	290		
N613	250	240		2,100

Note: Appropriate resistance factors need to be applied to the nominal unit side resistance and end bearing resistance presented.

#### 3.0 DRILLED, CAST-IN-PLACE, CONCRETE SHAFTS

#### 3.1 General

Recommendations are presented herein for rock socket drilled shafts for support of the proposed bridge structure foundations. A minimum 762-mm-diameter drilled shaft is recommended. The recommended design criteria are based on the AASHTO Load and Resistance Factor Design (LRFD) as presented in AASHTO LRFD Bridge Design Specifications (American Association of State Highway and Transportation Officials [AASHTO] 2010).

#### 3.2 Vertical Capacity

The axial compression capacity of the bridge drilled-shaft foundations was determined using the AASHTO LRFD rock socket design criteria, which determines the unit side resistance as a function of the unconfined compressive strength (UCS) of the rock and reduces it by an empirical amount to account for rock jointing. The unit side resistance determined cannot exceed the strength of the drilled-shaft concrete in shear, which is determined as a function of the UCS of the concrete.

Resistance to loads is developed by shear between the concrete of the drilled shaft and the wall of the drilled-shaft excavation. If tip resistance is considered in the analyses specialized cleaning of the bottom of the drilled-shaft foundation excavations will be necessary. Furthermore, the use of the maximum unit side resistance and the unit end bearing resistance is not recommended due to strain incompatibility of the two resistances. AMEC recommends unit side resistance or unit end bearing resistance be considered in the design, not both.

The maximum tip elevation of the rock sockets is the top of suitable rock elevation identified in Section 2.5, minus two drilled-shaft diameters.

#### 3.2.1 Strength and the Limit State

The drilled-shaft foundations were designed using side-wall shear in accordance with the AASHTO LRFD procedure developed by Horvath and Kenney (1979), as presented in equation



10.8.3.5.4b-1. This procedure considers the uniaxial UCS of the rock and a reduction factor to account for rock jointing. A resistance factor of 0.55 will need to be applied, per Table 10.5.5.2.4-1, for the Horvath and Kenney analytical procedure for side resistance. A resistance factor of 0.50 will need to be applied, per Table 10.5.5.2.4-1, for the O'Neill and Resse (1999) analytical procedure for end bearing.

#### 3.2.2 Service Limit State

The vertical resistance provided by the rock is a function of the movement between the drilled shaft and the surrounding rock mass. The elastic solutions of Carter and Kulhawy (1988) were used to compute the load-displacement behavior of the rock socket. The results of the analysis reveals that the full factored strength limit capacity of the rock socket will be achieved at a displacement of less than ½ inch. Therefore, a breakdown of service load capacities was not necessary.

## 3.2.3 Redundancy of Foundations

The resistance factors used for calculating the vertical drilled-shaft capacity may need to be modified depending upon the number of drilled shafts used at each foundation element or the redundancy of the foundations. Section 10.5.5.2.4 of AASHTO (2010) states "Where the resistance factors provided in [Table 10.5.5.2.4-1] are applied to a single shaft supporting a bridge pier, the resistance factor values in the Table should be reduced by 20 percent.

# 3.2.4 Group Effect - Axial

The minimum recommended center-to-center (CTC) pier spacing is 3.5 diameters. No axial capacity group reduction is recommended for drilled shafts founded in rock with this minimum spacing.

#### 4.0 DRIVEN PILES

#### 4.1 General

Recommendations are presented herein for driven piles founded on rock for support of the proposed bridge structure foundations at Bridge N613. The recommended design criteria are based on the AASHTO Load and Resistance Factor Design (LRFD) as presented in *AASHTO LRFD Bridge Design Specifications* (American Association of State Highway and Transportation Officials [AASHTO] 2010).

# 4.2 Vertical Capacity

The axial compression capacity of the bridge pile foundations was determined using the AASHTO LRFD end bearing on rock design criteria as outlined in the Canadian Geotechnical Society (1985), which determines the unit end bearing as a function of the UCS of the rock and reduces it by an empirical amount to account for rock jointing. Given the strong nature of the rock, the pile is not expected to penetrate into the rock sufficiently to develop side resistance and is therefore neglected.



Nominal pile bearing resistance should be verified in the field during pile installation using one of the methods outlined in AASHTO.

### 4.2.1 Strength and the Limit State

The pile foundations were designed using end bearing on rock design criteria as outlined in the Canadian Geotechnical Society (CGS) (1985), which determines the unit end bearing as a function of the UCS of the rock and reduces it by an empirical amount to account for rock jointing. A resistance factor of 0.50 will need to be applied, per Table 10.5.5.2.3-1, for the CGS analytical procedure for end bearing.

#### 4.2.2 Service Limit State

The settlement of the driven piles should be determined by the equivalent footing analogy as outlined in AASHTO. This should be completed once the pile group geometry and loading are determined.

#### 4.2.3 Redundancy of Foundations

The resistance factors used for calculating the vertical pile capacity may need to be modified depending upon the number of piles used at each foundation element or the redundancy of the foundations. Section 10.5.5.2.3 of AASHTO (2010) states "Where the resistance factors provided in [Table 10.5.5.2.3-1] are applied to a pile group of three or less supporting a bridge pier, the resistance factor values in the Table should be reduced by 20 percent.

#### 4.2.4 Group Effect - Axial

The minimum recommended center-to-center (CTC) pile spacing is 762 mm or 2.5 pile diameters. No axial capacity group reduction is recommended for piles founded in rock with this minimum spacing.

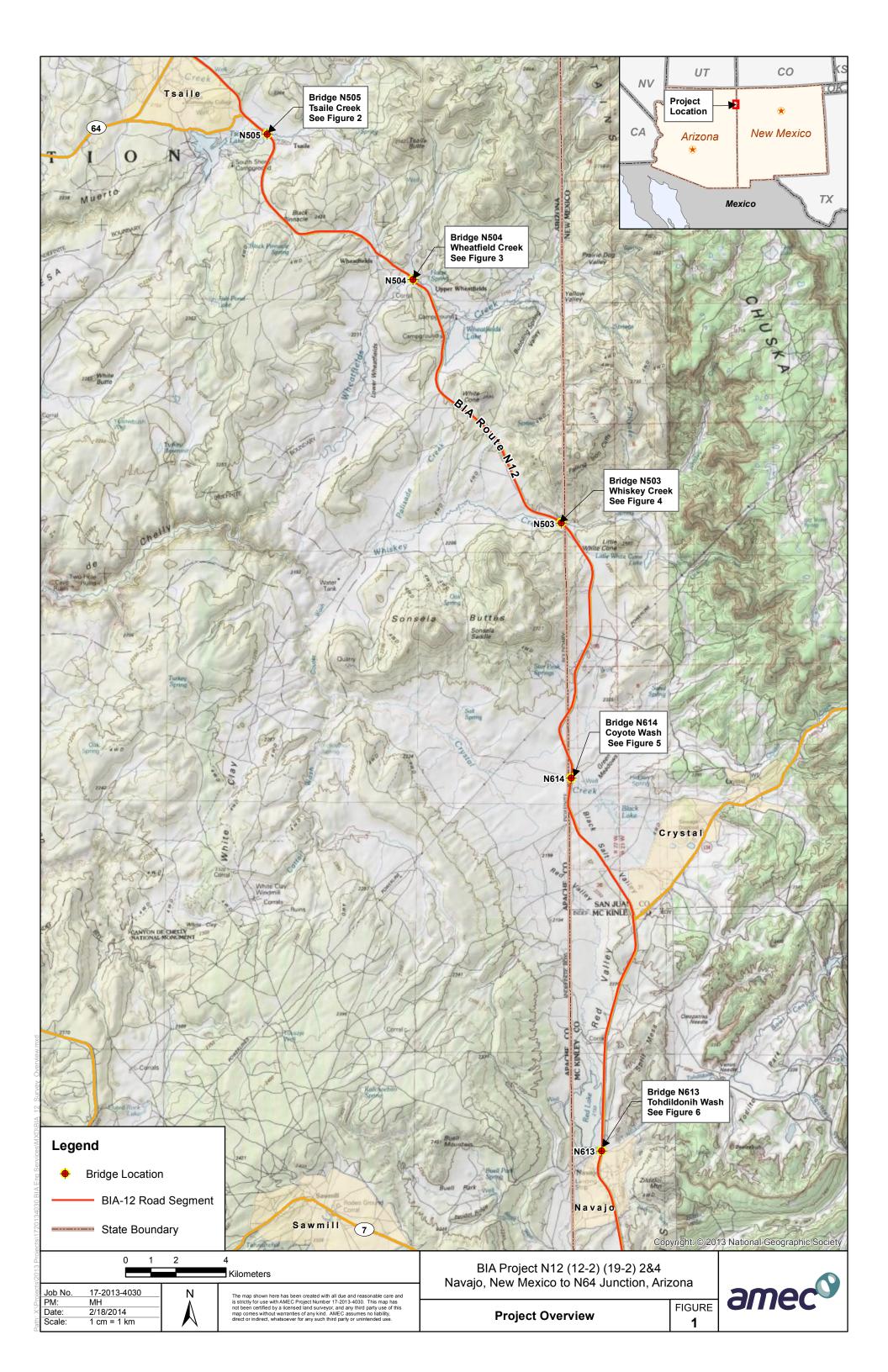


#### 5.0 REFERENCES

- Byers, V.P., 1980. Geologic Map and Sections of the Sonsela Butte 4 SE Quadrangle, Apache County, Arizona and San Juan and McKinley Counties, New Mexico. U.S. Geological Survey Open-File Report 80-788.
- O'Sullivan, R.B. and Beikman, H.M., 1963. Geology, Structure, and Uranium Deposits of the Shiprock Quadrangle, New Mexico and Arizona. U.S. Geological Survey Miscellaneous Geologic Investigations, Map I-345.
- Thaden, R.E., 1990. Geologic Map of the Buell Park Quadrangle, Apache County, Arizona and McKinley County, New Mexico. U.S. Geological Survey Geologic Quadrangle Map GQ-1649.



**FIGURES** 















# **APPENDIX A**

FIELD INVESTIGATION & BORING LOGS



# **TEST DRILLING EQUIPMENT AND PROCEDURES**

# <u>Description of Subsurface Exploration Methods</u>

<u>Auger Boring</u> Drilling through overburden soils is performed with 6 5/8-inch O.D., 3 1/4-inch I.D. hollow stem auger or 4 1/2-inch solid stem continuous flight auger. Carbide insert teeth are normally used on bits so they can penetrate soft rock or very strongly cemented soils. A CME-75 truck-mounted drill rig is used to advance the auger. The drill rigs are powered with six-cylinder Cummins diesel engines capable of delivering about 11.4 kN-m torque to the drill spindle. The spindle is advanced with twin hydraulic rams capable of exerting 90 kN (20,000 pounds) downward force.

Generally, refusal to penetration of the auger is adopted as top of the SGC or "river-run" material or harder bedrock, which require other techniques for penetration. Grab samples or auger cuttings may be taken as necessary. Standard penetration tests or 2.42-inch diameter ring samples are taken in conjunction with the auger borings as needed, with the sampling interval and type being indicated on the boring logs.

<u>Hammer Drill</u> Drilling with the Hammer drill is accomplished with a Drill Systems AP-1000 drill rig advancing a double-walled drive casing with a link-belt 180 diesel pile driving hammer, having a rated energy of 8,100 foot-pounds per blow. Where noted on the boring log, the hammer is equipped with a supercharger which can boost the energy to approximately 12,000 foot-pounds per blow. The supercharger is used only in portions of the boring where blow counts are relatively high. Cuttings are removed with compressed air by a reverse circulation process, and are collected in a cyclone from which grab samples are obtained. The drive casing is either 9-inch O.D. by 6-inch I.D. or 6 5/8-inch O.D. by 4-inch I.D. and employs an expendable bit of slightly larger diameter than the O.D. of the casing. Hammer blows required to advance the drive casing are recorded in 1-foot increments, as noted on the boring logs. Standard penetration tests or 2.42-inch diameter ring samples taken are noted on the boring logs.

Core Boring Rock core samples are retrieved using a CME-75 drill rig, SAITECH GH 3 rig or Burley 2500, 4500 or 4000. The GH 3 is a portable hydraulic core drill. The GH 3 is powered by a Kohler two-cylinder 25-horsepower engine. The hydraulics motor which feeds a two-speed transmission and powers the BW spindle. This unit has a 3-foot stroke and is hand-fed with a 2,000 pound push-pull capability. The GH 3 has the capability of drilling with either B- or N-size core steel using standard or wireline systems. N-size core is the preferred size and it has a nominal O.D. of about 2 inches. The Burley 2500 and 4500 series are portable hydraulic core drills. The 4500 series is capable of a track-mounted or skid-type chassis. The Burley 2500 and 4500 series are powered by 44 and 75 HP power units, respectively, provide up to 2,000 foot-pounds (ft.-lbs.) of torque and in excess of 1,000 revolutions per minute (RPM) of spindle speed. Both rigs are capable of retrieving either N- or H-sized core using wireline systems. The N-size core has a nominal O.D. of about 2 inches and the H-size of about 2.4 inches. The Burley 4000 is a track-mounted core drill.

The CME-75 utilizes a wireline core drilling system that takes N-size cores. Using the NQ wireline system, core is recovered quickly by retrieving the core-laden inner tube through the drill string.



# **TEST DRILLING EQUIPMENT AND PROCEDURES (Cont.)**

Sampling Procedures Dynamically driven tube samples are usually obtained at selected intervals in the borings by the ASTM D1586 test procedure. In many cases, 2-inch O.D., 1 3/8-inch I.D. samples are used to obtain the standard penetration resistance. "Undisturbed" samples of firmer soils are often obtained with 3-inch O.D. samples lined with 2.42-inch I.D. brass rings. The driving energy is generally recorded as the number of blows of a 140-pound, 30-inch free fall drop hammer required to advance the samples in 6-inch increments. However, in stratified soils, driving resistance is sometimes recorded in 2- or 3-inch increments so that soil changes and the presence of scattered gravel or cemented layers can be readily detected and the realistic penetration values obtained for consideration in design. These values are expressed in blows per 6 inches on the boring logs. "Undisturbed" sampling of softer soils is sometimes performed with thin walled Shelby tubes (ASTM D1587), pitcher samplers, Denison samplers or continuous CME samplers. Where samples are labeled and placed in watertight containers to maintain field moisture contents for testing. When necessary for testing, larger bulk samples are taken from auger cuttings. Also, representative samples are obtained from the cuttings from the hammer and Schramm drill rig.

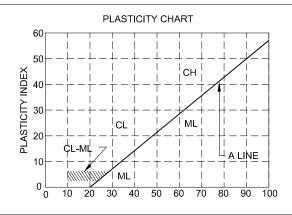
<u>Boring Records</u> Drilling operations are directed by our field engineer or geologist who examines soil recovery and prepares the boring logs. Soils are visually classified in accordance with the Unified Soil Classification System (ASTM D2487), with appropriate group symbols being shown on the boring logs.

#### UNIFIED CLASSIFICATION SYSTEM FOR SOILS

Soils are visually classified by the United Soil Classification System on the boring logs presente
Grain-size analysis and Atterberg Limits Tests are often performed on selected samples to aid in classification.
The classification system is briefly outlined on this chart. For a more detailed description of the system, see
"The Unified Soil Classification System" ASTM Designation: D2487

	ı	MAJOR DIVISION		GRAPH SYMBOL	GROUP SYMBOL	TYPICAL DESCRIPTION	
	GRAVELS (50% or less of coarse fraction passes No. 4 sieve)	CLEAN GRAVELS (Less than 5% passes No. 200 sieve)			GW	Well graded gravels, gravel-sized mixtures or sand-gravel-cobble mixture.	
					GP	Poorly graded gravels, gravel-sized mixtures or sand-gravel-cobble mixture.	
oll Sieve)		GRAVELS WITH FINES	Limits plot below "A" line & hatched zone on plasticity chart		GM	Silty gravels, gravel-sand-silt mixture.	
COARSE-GRAINED SOILS (Less than 50% passes No. 200 sieve)	(t	(More than 12% passes No. 200 sieve)	Limits plot below "A" line & hatched zone on plasticity chart		GC	Clayey gravels, gravel-sand-clay mixture.	
<b>ARSE-GR</b> . In 50% pas	SANDS (More than 50% of coarse fraction passes No. 4 sieve)	⊕ (a) CLEAN SANDS			SW	Well graded sands, gravelly sands.	
<b>CO</b> , (Less tha		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ses No. 200 sieve)		SP	Poorly graded sands, gravelly sands.	
		SAN re than 5i	SANDS WITH FINES	Limits plot below "A" line & hatched zone on plasticity chart		SM	Silty sands, sand-silt mixtures.
		(More than 12% passes No. 200 sieve)	Limits plot below "A" line & hatched zone on plasticity chart		sc	Clayey sands, sand-clay mixtures.	
v, °	SILTS LIMITS PLOT BELOW "A" LINE & HATCH ZONE ON PLASTICITY CHART	SILTS OF LOW (Liquid limit le			ML	Inorganic silts, clayey silts with slight plasticity.	
E-GRAINED SOIL % or more passe: No. 200 sieve)		SILTS OF HIGH (Liquid limit m			МН	Inorganic silts of high plasticity, silty soils, elastic silts.	
FINE-GRAINED SOILS (50% or more passes No. 200 sieve)	CLAYS CLAYS LIMITS PLOT BELOW "A" LINE & HATCH ZONE ON PLASTICITY CHART	CLAYS OF LOV (Liquid limit le			CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	
		CLAYS OF HIGI (Liquid limit m			СН	Inorganic clays of high plasticity, fat clays, silty and sandy clays of high plasticity.	

NOTE: Coarse-grained soils with between 5% to 12% passing the No. 200 sieve and fine-grained soils with limits plotting in the hatched zone on the plasticity chart to have dual symbol.



#### **DEFINITIONS OF SOIL FRACTIONS**

SOIL COMPONENT	PARTICLE SIZE RANGE
Boulders Cobbles Gravel Coarse gravel Fine gravel Sand Coarse Medium Fine Fines (silt or day)	Above 300mm (12in.) 300mm to 75mm (12in. to 3in.) 75mm (3in.) to No. 4 sieve 75mm to 19mm (3in to 3/4in.) 19mm (3/4in.) to No. 4 sieve No. 4 to No. 200 No. 4 to No. 10 No. 10 to No. 40 No. 40 to No. 200 Below No. 200 sieve



# TERMINOLOGY USED TO DESCRIBE THE RELATIVE DENSITY, CONSISTENCY OR FIRMNESS OF SOILS

The terminology used on the boring logs to describe the relative density, consistency or firmness of soils relative to the standard penetration resistance is presented below. The standard penetration resistance (N) in blows per foot is obtained by the ASTM D1586 procedure using 2" O.D., 1 3/8" I.D. samplers.

**Relative Density.** Terms for description of relative density of cohesionless, uncemented sands and sand-gravel mixtures.

<u>N</u>	Relative Density
0-4	Very loose
5-10	Loose
11-30	Medium dense
31-50	Dense
50+	Very dense

2. <u>Relative Consistency.</u> Terms for description of clays which are saturated or near saturation.

<u>N</u>	Relative Consistency	<u>Remarks</u>
0-2 3-4	Very soft Soft	Easily penetrated several inches with fist. Easily penetrated several inches with thumb.
5-8	Medium stiff	Can be penetrated several inches with thumb with moderate effort.
9-15	Stiff	Readily indented with thumb, but penetrated only with great effort.
16-30 30+	Very stiff Hard	Readily indented with thumbnail. Indented only with difficulty by thumbnail.

**Relative Firmness.** Terms for description of partially saturated and/or cemented soils which commonly occur in the Southwest including clays, cemented granular materials, silts and silty and clayey granular soils.

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<u>N</u>	Relative Firmness
0-4	Very soft
5-8	Soft
9-15	Moderately firm
16-30	Firm
31-50	Very firm
50+	Hard



# EXPLANATION OF CORE LOG PRESENTATION AND TERMINOLOGY FOR THE DESCRIPTION OF ROCK

**I.** ROCK QUALITY DESIGNATION (RQD). Percentage of rock core per core run which is relatively sound and unfractured and which is longer than 0.33 feet in length. Rock which is soft or weathered, closely jointed, or rock from which the core recovery is low, will have poor to fair RQD.

# II. <u>DISCONTINUITIES</u>

#### A. Spacing of Joints

<u>Code</u>	Spacing of Joints	<u>Descriptive Term</u>
1	Greater than 10 ft.	Very wide
2	3 ft 10 ft.	Wide
3	1 ft 3 ft.	Moderately close
4	0.2 ft 1 ft.	Close
5	Less than 0.2 ft.	Very close

# B. <u>Orientation of Joints</u>

Measurements presented represent dip angles from horizontal.

<u>Symbol</u> <u>Description</u>

Rdm Random - preferred orientation cannot be determined.

# C. Condition of Joints

# 1. Roughness

<u>Symbol</u>	Descriptive Term	<u>Properties</u>
Smth	Smooth	Appears smooth and is essentially smooth to the touch. May be slickensided.
Srgh	Slightly rough	Asperities on the fracture surfaces are visible and can be distinctly felt.
Mrgh	Medium rough	Asperities are clearly visible and fracture surface feels abrasive.
Rgh	Rough	Large angular asperities can be seen. Some ridge and high side angle steps evident.
VRgh	Very rough	Near-vertical steps and ridges occur on the fracture surface.



# EXPLANATION OF CORE LOG PRESENTATION AND TERMINOLOGY FOR THE DESCRIPTION OF ROCK

# C. Condition of Joints (cont.)

# 2. Presence or Absence of Fracture Filling Material

<u>Symbol</u>	Descriptive Term	<u>Definition</u>
Cln	Clean	No fracture filling material.
Stn	Stained	Coloration of rock only. No recognizable filling material.
Fld	Filled	Fracture filled with recognizable filling material

# III. <u>BEDDING</u>

<u>Symbol</u>	Descriptive Term	<u>Definition</u>
TL	Thinly laminated	Less than 0.01 ft.
L	Laminated	0.01 ft. to 0.04 ft.
ThB	Thinly bedded	0.04 ft. to 0.20 ft.
MB	Medium bedded	0.20 ft. to 2.00 ft.
TkB	Thickly bedded	More than 2.00 ft.

# IV. <u>DEGREE OF WEATHERING</u>

Symbol	Descriptive Term	<u>Properties</u>
Dec	Decomposed, generally so	il-like, can be crumbled by hand pressure.
HiW	Highly weathered, generall with difficulty by hand.	y rock-like, can be broken easily, but crumbles
MdW	Moderately weathered, fabrail, breaks only with difficu	ric stained rusty brown, can be indented by steel ulty.
SIW		discontinuities are weathered, coated, but only ass, generally not indented by steel nail.
UnW Ex Jts		nts, weathering limited to the surface of sh throughout but most joints show rusty stain
UnW Inc Jts		pints, rock mass and discontinuities are onal joints show rusty stain, practically no soil
UnW	<u>Unweathered</u> , rock mass u	nweathered; no staining or infilling.



# EXPLANATION OF CORE LOG PRESENTATION AND TERMINOLOGY FOR THE DESCRIPTION OF ROCK

#### V. HARDNESS

Descriptive Term **Properties** Very hard Cannot be scratched with knife or sharp pick. Breaking of hand specimens requires several hard blows of geologist's pick. Hard Can be scratched with knife or pick only with difficulty. Hard blow of hammer required to detach hand specimen. Moderately hard Can be scratched with knife or pick. Gouges or grooves to 3 inch deep can be excavated by hard blow of point of a geologist's pick. Hand specimens can be detached by moderate blow. Moderately soft Can be grooved or gouged 1/16 inch deep by firm pressure on knife or pick point. Can be excavated in small chips to pieces about 1 inch maximum size by hard blows of the point of a geologist's pick. Soft Can be gouged or grooved readily with knife or pick point. Can be excavated in chips to pieces several inches in size by moderate blows of a pick point. Small thin pieces can be broken by finger pressure. Very soft Can be carved with knife. Can be excavated readily with point of pick. Pieces 1 inch or more in thickness can be broken with finger pressure. Can be scratched readily by fingernail.

#### VI. <u>MISCELLANEOUS ABBREVIATIONS</u>

<u>Symbol</u>	<u>Description</u>	<u>Symbol</u>	<u>Description</u>
Bkn Brc Band Qtz Calc Cem Frct Fgd	Broken Brecciated Banded Quartz Calcite Cemented Fractured Fine-Grained	Incl Mgd Mod Wkly Slicks Strong SZ Gog	Inclusions Medium-Grained Moderately Weakly Slickensides Strongly Shear Zone Gouge
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4001370.138

**LOCATION** JOB NO. 17-2013-4030 **DATE** 10/6/13 E. 675659.5221 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2231.1m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log ШШ Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION SC-SM moist SILTY CLAYEY SAND, some fine grained, subangular gravel, predominantly fine to medium grained sand, low plasticity, calcareous firm mix of green, gray, black & reddish-brown note: reacts to HCI S 12-13-CL SANDY CLAY WITH GRAVEL, some coarse grained gravel, calcareous sandstone cobble, 18 moist 3 medium plasticity, brown with green spots firm note: reacts to HCI CL-ML U 28-35-4 SILTY CLAY WITH SAND, trace gravel, some 50/ fine grained sand, low plasticity, brown moist 152mm 16-19note: does not react with HCI 5 very firm 25  $\nabla$ ML SANDY SILT, trace fine grained sand, 6-11calcareous, nonplastic 13 wet 6 note: reacts to HCI firm GM SILTY GRAVEL WITH SAND, some silt, S 28-33considerable fine grained, subangular gravel, 44 predominantly fine to medium grained sand, wet 8 nonplastic, green & black hard note: does not react with HCI 50/ 76mm Stopped Auger at 8.8m 9 Began HQ Coring at 8.8m 10 11 12 13 14 15 GROUNDWATER

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	5.5		10-6-13
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample. LOG OF TEST BORING NO.N503-B-1



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-6-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4001370.138 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 675659.5221 Sample Type 2231.1m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 2 5 3 4 Rock Type & Remarks Began HQ Coring at 8.8m 10/6 HQ 20 95 0 SRgh TL MdW CHINLE FORMANTION HQ4.0 Cln to L to CALCAREOUS SILTSTONE, moderately soft to SIW 8.4 HQ 95 35 moderately hard, reddish-brown with grayish-green reduction spots (2mm to 13mm) note: some irregularly-shaped healed fractures 10 note: calcareous nodular zones 9.0 85 75 SIW HQ note: increase in nodules & reduction spots below 25249 11.3m -11 12 8.8 HQ 100 70 note: majority of breaks/discontinuites occur on bedding ] planes (near horizontal) -13 22.6 HQ 30100 100 100 75 note: slight color change, more pinkish, numerous nodules at 13.7m 14 note: low RQD values in zones due to mechanical breaks 16.8 HQ 100 65 note: discontinuity spacing resultant from mechanical 15 breaks & relatively soft rock mass in some zones Stopped HQ Coring at 15.4m

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**BORING OPERATION** 

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Page 2 of 2



4001377.29 **LOCATION** JOB NO. 17-2013-4030 **DATE** 10/4/13 675666.1267 E. CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2232.6m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log E Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION SC slightly moist **Asphalt** CLAYEY SAND, trace silt, predominantly fine grained sand, calcareous, low to medium firm plasticity, brown note: reacts to HCI S 12-12-CL-ML SILTY CLAY, occasional fine grained gravel, 12 slightly moist 2 predominantly medium to fine grained, subangular sand, low to medium plasticity, firm reddish-brown S 10-15-CI note: does not react with HCI 20 SANDY CLAY, trace silt, trace predominantly very firm fine grained gravel, considerable fine to medium 4 grained sand, medium plasticity, reddish-brown  $\nabla$ U 24-50/ 1855 note: does not react with HCI 5 152mm 6 GM S 35-50/ SILTY GRAVEL WITH SAND, some to considerable predominantly fine to medium <del>152mm</del> wet grained sand, fine to coarse grained gravel, nonplastic, red & green hard note: does not react with HCI 9-10-SM S SILTY SAND, some clay, predominantly fine 8 30 wet grained sand, nonplastic very firm note: does not react with HCI 50/ ML SANDY SILT, trace clay, some fine grained S sand, low plasticity, reddish-orange 51mm slightly moist 10 note: does not react with HCI hard 50/ CL-ML SILTY CLAY, some clay, considerable silt, S 11 calcareous, medium plasticity, light 76mm slightly moist reddish-brown hard note: reacts to HCI 12 <del>50/</del> 102mm Stopped Auger 11.9m Sampler refused at 12.0m 13 Began HQ Coring at 11.9m 14 15 **GROUNDWATER** SAMPLE TYPE

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	4.6	09:30	10-4-13
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A - Auger cuttings; NR-No Recovery

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N503-B-2 U - 76mm O.D. 61mm I.D. tube sample.



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-4-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling Boring Operation and Drill Rate (min/meter) Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Rock Quality Designation (RQD) Spacing Orientation **N.** 4001377.29 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 675666.1267 Sample Type % Core Recovery 2232.6m **ELEVATION** Condition Depth in [ Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 11.9m 50 100 10/4 HQ 0 N/A SIW CHINLE FORMANTION TL 12 IQ22.0 to L to CALCAREOUS SILTSTONE, moderately soft to NONE MdW 21.0 HQ 100 20 moderately hard, reddish-brown with greenish-gray note: nodules are lighter & grayer color of the brown silt 8.2 HQ 100 90 -13 8.2 HQ 100 14 15 7.8 90 80 note: some turbidikes in zones below 15.2m 12844 note: clay-rich zones 16 9.3 100 HQ 95 17 18 Stopped HQ Coring at 18.3m note: low RQD values in zones due to mechanical breaks 19 note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones

	GROUNDWATER					
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BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Page 2 of 2



4001347.19

**LOCATION** JOB NO. 17-2013-4030 **DATE** 10/16/13 E. 675688.7639 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2233.0m SURFACE ELEV. Unified Soil Classification Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log m Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION CL-ML moist SANDY SILTY CLAY, occasional fine grained, subangular gravel, considerable predominantly fine grained sand, low plasticity, brown moderately firm note: does not react with HCI S 3-5-7 2 S 4-6-8 MI SANDY SILT, trace clay, considerable predominantly fine grained sand, low plasticity, slightly moist reddish-brown 4 moderately firm note: does not react with HCI 51 5  $\nabla$ 6 GP-GM S 10-18-SANDY GRAVEL WITH SILT, considerable predominantly fine grained sand, angular to 22 wet subangular gravel, nonplastic, grayish-brown very firm note: does not react with HCI SP-SM SAND WITH SILT & GRAVEL, some fine S 4-6-9 8 grained, subangular to subrounded gravel, wet predominantly medium to fine grained sand, nonplastic, gray firm 9 note: does not react with HCI SM S 24-50/ SILTY SAND WITH GRAVEL, considerable 102mm hard predominantly fine grained gravel, considerable 10 predominantly fine to medium grained sand, nonplastic, brown S 25-50/ SC-SM note: does not react with HCI 11 102mm SILTY CLAYEY SAND WITH GRAVEL, slightly moist considerable predominantly fine grained gravel, predominantly fine to coarse grained sand, low 12 plasticity, brown hard note: does not react with HCI 13 Stopped Auger at 10.7m Sampler refused at 10.9m Began HQ Coring at 10.7m 14 15 **GROUNDWATER** Page 1 of 2

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	5.6	16:20	10-16-13
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SAMPLE TYPE

A - Auger cuttings; NR-No Recovery

T - 25mm O.D. thin-walled tube sample

S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N503-B-3 U - 76mm O.D. 61mm I.D. tube sample.



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 10-17-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4001347.19 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 675688.7639 Sample Type % Core Recovery 2233.0m **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 2 5 3 4 Rock Type & Remarks Began HQ Coring at 10.7m 10/17 HQ 0 100 NO RECOVERY NO RECOVERY MdW CHINLE FORMANTION HQ LT CALCAREOUS SILTSTONE, moderately soft to 5.8 -11 moderately hard, brown to dark brown note: chemical reduction spots, some clay in zones, brown to reddish-brown 75 HQ 0 **BROKEN** note: small 76mm to 127mm thick zones of calcified 15.5 12 nodules from 11.7m to 15.4m 11.6 HQ 75 80 20 SIW note: occasional near-vertical calcite-healed fracture to at 13.7m MdW 18623 note: fracture surfaces calcite filled or stained at 14.0m 13 note: soft (decomposed zone to clay) from 15.1m to 15.2m **BROKEN** note: hard to very hard silicified zone from 15.5m to 16.0m 12.0 HQ 50 SRgh 15 14 note: occasional thin turbidite zone 16.0m **BROKEN** 15 Dec 24.1 SIW HQ 70 30 Smth Stn 16 40142 Stopped HQ Coring at 16.8m note: low RQD values in zones due to mechanical 17 breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones

	GROUNDWATER					
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BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Page 2 of 2



4001355.992

**LOCATION** JOB NO. 17-2013-4030 **DATE** 10/18/13 E. 675692.5248 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2231.7m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log mm Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION SC slightly moist **Asphalt** CLAYEY SAND, predominantly fine grained sand, low plasticity, brown note: does not react with HCI SM SILTY SAND, rare cobbles, considerable silt, S 4-8-10 predominantly fine grained sand, trace slightly moist predominantly fine grained gravel, nonplastic, firm 3 note: strong reaction with HCI Īυ 55 1885 10 4 GM S 3-3-6 SILTY SANDY GRAVEL, considerable predominantly fine to medium grained sand, moist predominantly fine grained gravel, nonplastic,  $\nabla$ moderately firm 6 note: does not react with HCI SM S 12-7-7 SILTY SAND, considerable silt, predominantly wet fine grained sand, nonplastic, brown moderately firm note: does not react with HCI SP SAND WITH GRAVEL, considerable S 4-9-10 8 predominantly fine to coarse grained, angular to wet subangular gravel, predominantly fine to medium grained sand, nonplastic, dark gray very stiff 9 note: does not react with HCI SM H 41 SILTY SAND WITH GRAVEL, some to wet considerable angular to subangular gravel, 10 predominantly medium grained sand, hard nonplastic, light brown note: does not react with HCI 11 Stopped Auger at 10.5m Began HQ Coring at 10.5m 12 13 14 15 **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	5.5	12:30	10-18-13
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SAMPLE TYPE

A - Auger cuttings; NR-No Recovery

T - 25mm O.D. thin-walled tube sample

Page 1 of 2



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-18-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4001355.992 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 675692.5248 Sample Type 2231.7m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Bagan HQ Coring at 10.5m 10/18 IQ14.0 HQ 0 100 NO RECOVERY NO RECOVERY 0 SRgh L to CHINLE FORMANTION TL Cln 12.6 HQ 65 25 CALCAREOUS SILTSTONE, moderately hard, reddish-brown -11 note: greenish-gray reduction spots 12 note: clay-rich zones 17.4 HQ 90 80 note: calcium carbonate nodules up to 2.5mm long below 11.0m 13 31202 10/19 100 95 95 HQ 20.1 14 15 22.2 HQ 90 85 note; very hard silicified zone & turbidite with angular clasts from 16.0m to 16.3m 32531 16 Stopped HQ Coring at 16.8m 17 note: low RQD values in zones due to mechanical breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones

	GROUNDWATER			
	DEPTH (m)	HOUR	DATE	
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**BORING OPERATION** 

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Page 2 of 2

LOG OF TEST BORING NO. N503-B-4



4011025.16 **LOCATION DATE** 9-18-13 & 9-19-13 JOB NO. 17-2013-4030 E. 669669.0039 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** SURFACE ELEV. 2219.3m Unified Soil Classification Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log Blows per 152 mm Sample REMARKS VISUAL CLASSIFICATION SM moist 152mm Asphalt SILTY SAND, rare predominantly fine grained firm to hard gravel, considerable predominantly fine grained sand, nonplastic, grayish-brown 2 U 1912 11 41 note: brown, reacts with HCI at 2.3m 3 4 note: color change to dark grayish-brown S 15-18at 4.6m, end gravel S 15-38- $\nabla$ 43 23 ML SANDY SILT, some fine grained sand, U 8 nonplastic, light brown wet U NR firm note: reacts with HCI SP GRAVELLY SAND, trace silt, light brown slightly moist note: does not react with HCI 10 hard 11 12 23-50/ CL CLAY, some silt, trace fine grained sand, medium plasticity, reddish-brown 76mm moist 13 hard note: mild reaction with HCI note: possible siltstone beginning at 12.2m S 24-50/ 14 76mm 15 **CLAY WITH SAND** 47-50/ CL 76mm

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	6.4		9-18-13
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**GROUNDWATER** 

SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-1 U - 76mm O.D. 61mm I.D. tube sample.

Navajo, New Mexico to N64 Junction, Arizona



4011025.16 LOCATION **DATE** 9-18-13 & 9-19-13 JOB NO. 17-2013-4030 E. 669669.0039 CME-85 Buggy Mounted **RIG TYPE** 203mm Hollow Stem Auger **BORING TYPE** 2219.3m SURFACE ELEV. Unified Soil Classification Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 Graphical Log **DATUM** шш Blows per 152 mn **REMARKS** VISUAL CLASSIFICATION CLAY WITH SAND, some to considerable 16 CL predominantly fine to medium grained sand, medium plasticity, reddish-brown U 28-50/ 17 note: does not react with HCI 76mm 18 50/ MH CLAYEY SILT, considerable clay, medium S 140mm plasticity, reddish-brown moist 19 hard note: no reaction to HCI note: color change to brown at 19.8m 20 21 S 50/ note: color change to brown to reddish-brown 140mm at 21.3m 22 U 38-50/ 23 152mm 24 S 50/ note: color change to brown at 24.4m 102mm 25 26 50/ CH SILTY CLAY, high plasticity, brown 140mm moist note: does not react with HCI 27 hard U 50/ 140mm 28 29 МН CLAYEY SILT, high plasticity, reddish-brown 50/ 140mm slightly moist note: does not react with HCI 30 hard Stopped Auger at 30.5m 140mm 31 Sampler refused at 30.6m GROUNDWATER

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	6.4		9-18-13
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 2 of 2

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-1 U - 76mm O.D. 61mm I.D. tube sample.



4011028.254 **LOCATION** JOB NO. 17-2013-4030 **DATE** 9/21/13 669673.9659 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2218.6m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log Blows per 152 mm Sample REMARKS VISUAL CLASSIFICATION SM slightly moist 152mm Asphalt SILTY SAND, predominantly medium grained firm to hard sand, nonplastic, dark grayish-brown note: no reaction with HCI 6-11-S note: mild reaction with HCI, color change to 11 black to brown at 1.5m 2 3 U 60 note: little to no reaction with HCl at 3.0m note: predominantly fine grained sand 4 S 11-22note: mild to moderate reaction with HCI 25 at 4.6m 6 S 13-13note: mild reaction with HCI, color change to dark brown at 6.1m 14  $\nabla$ S 11-14note: color change brown at 7.6m 8 11 9 H 33 note: considerable subrounded gravel, predominantly medium grained sand, light brown, no reaction with HCL at 9.1m 10 note: some rounded gravel, predominantly S 22-50/ 11 140mm medium to fine grained sand, trace micaceous siltstone at 10.7m 12 50/ 140mm ML CLAYEY SILT, nonplastic, purple to reddish-brown 13 note: very mild reaction with HCI 50/ 14 note: possible siltstone beginning at 12.5m <u>127mm</u> 15 50/ S 127mm **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	7.6		9-21-13
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-2 U - 76mm O.D. 61mm I.D. tube sample.



4011028.254

LOCATION **DATE** 9/21/13 JOB NO. 17-2013-4030 E. 669673.9659 CME-85 Buggy Mounted **RIG TYPE** 203mm Hollow Stem Auger **BORING TYPE** 2218.6m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 Graphical Log **DATUM** Blows per 152 mm **REMARKS** VISUAL CLASSIFICATION 16 ML **CLAYEY SILT**, continued  $\simeq_{\mathsf{S}}$ 50/ 17 140mm 18 III U 50/ note: color change to brown at 18.3m 127mm 19 S 50/ СН SILTY CLAY, high plasticity, brown 20 140mm moist note: no reaction with HCI hard 21 IJ 50/ МН CLAYEY SILT, brown to reddish-brown 140mm 22 note: mild reaction with HCI moist hard symp s23 50/ note: no reaction with HCI, color change to 152mm brown at 22.9m 24 S 50/ 140mm 25 26 ΨU 50/ 127mm 27 50/ 127mm 28 Stopped Auger at 28.2m 29 30 31 **GROUNDWATER** SAMPLE TYPE Page 2 of 2

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	7.6		9-21-13
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T - 25mm O.D. thin-walled tube sample

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-2 U - 76mm O.D. 61mm I.D. tube sample.



4010994.663 **LOCATION DATE** 9-17-13 & 9-18-13 JOB NO. 17-2013-4030 E. 669688.928 CME-85 Buggy Mounted **RIG TYPE** 203mm Hollow Stem Auger **BORING TYPE** 2219.0m SURFACE ELEV. Unified Soil Classification Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 | Graphical | Log DATUM Blows per 152 mm Sample REMARKS VISUAL CLASSIFICATION CL-ML slightly moist SANDY SILTY CLAY, occasional fine grained gravel, considerable predominantly fine grained hard sand, low plasticity, brown U 12-22note: moderate reaction with HCI 20/ 127mm note: almost no reaction with HCL at 1.5m 12-29-2 50/ 127mm SC S 12-26-**CLAYEY SAND WITH GRAVEL**, some coarse grained gravel, predominantly fine 50 moist grained sand, medium plasticity, purple 4 note: does not react with HCI hard S 12-36-50/ **76mm** 6 SM S 15-15-SILTY SAND, predominantly fine grained 23 sand, considerable silt, nonplastic, brown note: well graded, fine grained sand moist U 31  $\nabla$ very firm note: does not react with HCI 8 S 12-15-23 10 S 31-50/ ML CLAYEY SILT, low plasticity, reddish-brown 11 127mm moist note: slight reaction with HCI hard 12 42-50/ S note: no reaction with HCI, color change to red 127mm at 12.2m 13 note: possible siltstone beginning at 10.7m U 30-50/ 14 <u>76mm</u> 15

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	7.6		9-17-13
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GROUNDWATER

SAMPLE TYPE

A - Auger cuttings; NR-No Recovery

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-3 U - 76mm O.D. 61mm I.D. tube sample.

Navajo, New Mexico to N64 Junction, Arizona



4010994.663

**LOCATION DATE** 9-17-13 & 9-18-13 JOB NO. 17-2013-4030 669688.928 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2219.0m SURFACE ELEV. Unified Soil Classification Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log шш Blows per 152 mn REMARKS VISUAL CLASSIFICATION 16 ML moist CLAYEY SILT, continued, dark brown hard S 23-50/ note: medium plasticity, reddish-brown at 16.8m 17 102mm 18 U 24-50/ note: some medium to fine grained sand, color 127mm change to red at 18.3m 19 S 24-50/ МН **CLAYEY SILT**, high plasticity, reddish-brown 20 127mm wet note: does not react with HCI hard 21 S 50/ 140mm 22 S 40-50/ 23 ML CLAYEY SILT WITH SAND, some fine **76mm** wet grained sand, low plasticity, red hard note: does not react with HCI 24 U 30-50/ MH **CLAYEY SILT**, medium plasticity, 127mm reddish-brown 25 moist note: does not react with HCI hard 26 S 40-50/ CH SILTY CLAY, high plasticity, brown to light red 127mm wet note: does not react with HCI hard 27 S 38-50/ 127mm 28 29 S 48-50/ 127mm 30 U 28-50/ <del>102mm</del> Stopped Auger at 30.5m 31 Sampler refused at 30.6m GROUNDWATER

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	7.6		9-17-13
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 2 of 2

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-3 U - 76mm O.D. 61mm I.D. tube sample.

Navajo, New Mexico to N64 Junction, Arizona



4010998.746 **LOCATION** JOB NO. 17-2013-4030 **DATE** 9/20/13 E. 669695.8424 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2217.5m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log ШШ Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION SM slightly moist 152mm Asphalt SILTY SAND, some calcium carbonate, nonplastic, dark grayish-brown CL SANDY CLAY, trace silt, considerable S 5-9-6 predominantly fine grained sand, medium slightly moist plasticity, brown 2 moderately firm note: moderate reaction with HCI S 5-19-SM SILTY SAND, trace clay & gravel, 29 predominantly fine grained sand, nonplastic moist very firm 4 note: no reaction with HCI at 4.6m 59 1962 8 6 S 5-29 hard note: predominantly fine grained sand, moderate reaction with HCI at 6.1m 28  $\nabla$ SP-SM SAND WITH SILT & GRAVEL, considerable S 12-22-8 predominantly fine grained gravel, 29 wet predominantly fine grained sand, nonplastic, light brown to brown hard to firm 9 H 26 note: predominantly medium to fine grained sand, dark brown at 9.1m 10 note: does not react with HCI 9-22-S 11 30 12 12-50/ ML CLAYEY SILT, medium plasticity, 152mm moist reddish-brown 13 hard note: mild reaction with HCI note: possible siltstone beginning at 12.2m S 24-50/ 14 140mm 15 50/ **GROUNDWATER** SAMPLE TYPE

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	7.6		9-20-13
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T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-4



4010998.746 **LOCATION DATE** 9/20/13 JOB NO. 17-2013-4030 E. 669695.8424 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2217.5m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 Graphical Log **DATUM** Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION 152mm 16 ML moist **CLAYEY SILT**, continued hard note: reddish-brown Ш<u>U</u> 50/ 17 140mm 18  ${f >\!\!\! \leq}_{f S}$ 50/ note: marbled brown colors at 18.3m 152mm 19  $\bowtie_{\mathsf{S}}$ 50/ note: moderate reaction with HCl at 19.8m 20 152mm 21 S 50/ note: little to no reaction with HCl, color change 140mm to brown at 21.3m 22 23 U 13-28note: no reaction with HCI at 22.9m 50/ 102mm 24 S 50/ 127mm 25 26 S 50/ 102mm 27 **∥∪ 28-50/** 127mm 28 29 50/ 152mm 30 S 50/ <del>152mm</del> Stopped Auger at 30.5m 31 Sampler refused at 30.6m

	DEPTH (m)	HOUR	DATE
$\bar{\nabla}$	7.6		9-20-13
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GROUNDWATER

SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 2 of 2

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N504-B-4 U - 76mm O.D. 61mm I.D. tube sample.

Navajo, New Mexico to N64 Junction, Arizona



4016770.864 **LOCATION DATE** 10/3/13 JOB NO. 17-2013-4030 663792.2072 E. CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2168.9m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION SC **CLAYEY SAND WITH GRAVEL,** slightly moist predominantly fine grained sand, calcareous, low to medium plasticity, grayish-brown hard note: moderate reaction with HCI U 25-50/ 140mm note: considerable silt GC **CLAYEY GRAVEL WITH SAND, trace silt,** 50/ 102mm considerable fine grained sand, predominantly slightly moist coarse grained gravel 4 hard note: does not react with HCI 5 Stopped Auger at 4.3m Began HQ Coring at 4.3m 6 7 8 10 11 12 13 14 15 **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample. LOG OF TEST BORING NO.N505-B-1



CME-85 Buggy Mounted **RIG TYPE** JOB NO. 17-2013-4030 10-3-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4016770.864 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 663792.2072 Sample Type 2168.9m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 45 Rock Type & Remarks 4 Began HQ Coring at 4.3m 100 HQ 75 25 VTb CHINLE FORMANTION SRgh HQ 0.3 Fgn SANDSTONE, fine grained, well sorted, moderately hard to hard, friable note: quartz arenite, fine grained (colorless & tan) clear quartz, slight SiO2 overgrowths, light tan to medium tan, 4.2 HQ 65 30 gray tan TL SRgh Stn to L note: bedding dips range from 7° to 15° occ Mgn to note: some clay filled worm burroughs Cgn zones note: some fracture surfaces stained with iron-oxide 43733 4.2 HQ 100 0 MRgh to to L note: some fabric stained in zones with iron-oxide SRgh Stn 8 SRgh SIW Cln 4.0 HQ 100 25 steplike. features note: some worm burroghs below 9.0m J note: occasional medium to coarse grained zones thoughout 3.5 HQ 80 30 note: low to zero RQD values due to mechanical breaks 10 along bedding planes SRgh TL to L Insteplike note: water used while coring, therefore unknown if 40539 featgroundwater encountered Stopped HQ Coring at 10.7m note: low RQD values in zones due to mechanical 11 breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones

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BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Navajo, New Mexico to N64 Junction, Arizona



4016778.682 **LOCATION DATE** 10/3/13 JOB NO. 17-2013-4030 E. 663798.5613 CME-85 Buggy Mounted **RIG TYPE** 203mm Hollow Stem Auger **BORING TYPE** 2168.7m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION SC slightly moist **CLAYEY SAND WITH GRAVEL**, trace subangular to subrounded gravel, predominantly fine grained sand, low to medium very firm to hard plasticity, light grayish-tan note: moderate reaction with HCl S 17-17-14 note: increase plasticity & increase in clay U 60 3 note: little to no reaction with HCI, color change to light green S 50/ 4 Stopped Auger at 4.3m Began HQ Coring at 4.3m 5 6 7 8 10 11 12 13 14 15 GROUNDWATER

	DEPTH (m)	HOUR	DATE
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SAMPLE TYPE

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N505-B-2 U - 76mm O.D. 61mm I.D. tube sample.

T - 25mm O.D. thin-walled tube sample

Page 1 of 3



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-3-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4016778.682 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 663798.5613 Sample Type 2168.7m % Core Recovery **ELEVATION** Condition Depth in [ Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks -4 Began HQ Coring at 4.3m 10/3 HQ 5.3 HQ 80 100 45 None L to SIW CHINLE FORMATION ThB SANDSTONE, quartz arenite, well sorted, medium to MdW Fgn 2.4 HQ 0 NO RECOVERY NO RECOVERY fine grained, moderately hard to hard, trace red & black to (opaque) grains, predominate colorless & yellow clear Mgn quartz, grayish-tan to tan note: cross-bedded in zones 4.0 HQ 5 0 Fgn NONE note: predominantly fine grained sandstone at 6.2m NO RECOVERY NO RECOVERY note: some variably-oriented partially open fractures at 7.3m 1.6 HQ 25 70 MB NONE in zones note: some small diameter roots along fracture bedding surfaces 8.8m ThB 3.0 to L HQ 5 with NO RECOVERY NO RECOVERY note: low to no RQD values due to poor recovery MB percentages and/or mechanical breaks along bedding zones planes at 9.4m -10 note: occasional black manganese & brown, iron-oxide 4.0 90 20 SIW HQ SRgh L to staining on fabric & fracture surfaces below 9.1m 11 Stn TL to MdW

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**BORING OPERATION** 

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 10-3-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4016778.682 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 663798.5613 Sample Type 2168.7m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 3 4 H 45 Rock Type & Remarks 10/3 HQ 4.0 39061 100 SIW **CHINLE FORMATION** part L to 12 Stn ThB SANDSTONE, continued SRgh Cln part note: occasional worm burroughs from 12.3m to 13.4m 3.5 HQ 95 80 & 14.6m to 15.0m -13 33827 note: dark brown alternating laminea 3mm to 6mm thick below 13.6m 4.8 HQ 90 0 14 MdW Smth to SRgh Stn Stopped HQ Coring at 15.4m note: low RQD values in zones due to mechanical breaks 16 note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones note: water used while coring, therefore unknown if groundwater encountered 17 18 19

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	DEPTH (m)	HOUR	DATE		
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**BORING OPERATION** 

D - Disturbed Bulk Sample

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

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4016751.141 N. **LOCATION DATE** 9/24/13 JOB NO. 17-2013-4030 E. 663816.675 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2169.5m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION CL slightly moist SANDY CLAY WITH GRAVEL, some fine grained gravel to rare moderately calcareous, considerable predominantly fine grained sand, firm to hard medium plasticity, light grayish-tan S 6-8-12 note: decrease gravel, brown, medium plasticity note: does not react with HCI 3 ⊒Ш 50/ 127mm 4 Stopped Auger at 4.4m Began HQ Coring at 4.4m 5 6 7 8 10 11 12 13 14 15 GROUNDWATER Page 1 of 2

	DEPTH (m)	HOUR	DATE
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample. LOG OF TEST BORING NO.N505-B-3



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 9-24-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4016751.141 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 663816.675 Sample Type 2168.5m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 4.4m 50 100 9/24 HQ 0 SRgh ThB CHINLE FORMATION HQ Stn to L SANDSTONE, quartz arenite, well sorted, medium to Fgn fine grained, moderately hard to hard, trace red & black 4.0 HQ 70 25 note: worm burroghs & clay fill to 5.5m note: considerable micaceous laminae SIW note: some predominantly high-angle partially open -6 fractures at 6.1m 42314 note: bedding dips variable from subhorizontal up to 15° 4.0 100 20 HQ MRgh Т Steplike Features to Partinote: considerable brown, iron-oxide staining along some fracture surfaces & in fabric in zones at 7.6m Stn 3.8 HQ 95 50 MB note: clay-rich laminae from 9.0m to 9.3m note: considerable black, manganese-oxide staining on trace surfaces from 9.6m to 10.2m note: some worm burroughs below 10.2m 4.0 HQ 100 20 note: low RQD values in zones due to mechanical breaks 10 note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones 24694 note: water used while coring, therefore unknown if groundwater encountered -11 Stopped HQ Coring at 11.1m

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CDOLINDWATED

BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Navajo, New Mexico to N64 Junction, Arizona



4016759.232 **LOCATION DATE** 9/22/13 JOB NO. 17-2013-4030 663822.9862 E. CME-85 Buggy Mounted **RIG TYPE** 203mm Hollow Stem Auger **BORING TYPE** 2168.1m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION CL SANDY CLAY, trace fine grained, rounded gravel, predominantly medium to fine grained sand, medium plasticity, dark brown note: moderate reaction with HCI 36 SM SILTY SAND, trace subrounded gravel, considerable silt, predominantly fine grained sand, nonplastic, tan firm 3 note: strong effervesence with HCI Stopped Auger at 2.7m Began HQ Coring at 2.7m 4 5 6 7 8 10 11 12 13 14 15 GROUNDWATER SAMPLE TYPE

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$		none	
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T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample.
LOG OF TEST BORING NO.N505-B-4



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 9-23-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 4016759.232 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 663822.9862 Sample Type 2168.1m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 2.7m 100 9/23 HQ 95 0 SRgh Stn SIW CHINLE FORMATION L HQ 4.7 SANDSTONE, quartz arenite, well sorted, medium Fgn grained, moderately hard to hard, clear white gray & tan 3.8 HQ 100 0 stained grains, light gray to tan Smth note: darker tan to light brown hematite stain 13mm to Stn 25mm thick from 3.5m to 5.6m TL SRgh Stn ThB UnW note: clay infilling along bedding planes from to L Jts 4.3m to 4.6m 4.0 HQ 80 0 MRgh Stn note: bedding planes generally dipping at 10° to 15° at 5.2m SIW Mgn TL Smth UnW note: 1.6mm to 3.2mm pinkish-brown to green laminae Jts HQ 90 35 at 6.0m HQ note: brown zones & micaceous-rich bedding planes from 6.3m to 6.7m note: low to no RQD values due to mechanical breaks 3.8 HQ 100 25 along bedding planes 7.6m 8 note: some predominate high-angle partially open fractures 8.2m note: clay infilling along bedding planes from Rgh Cln SIW 8.7m to 9.0m Mgn note: water used while coring, therefore unknown if 37604 groundwater encountered Fgn Stopped HQ Coring at 9.3m note: low RQD values in zones due to mechanical note: discontinuity spacing resultant from mechanical 10 breaks & relatively soft rock mass in some zones

	GROUNDWATER				
	DEPTH (m)	HOUR	DATE		
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BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring

S - 51mm O.D./35mm I.D. Tube Sample D - Disturbed Bulk Sample



3976367.143

**LOCATION DATE** 10/19/13 JOB NO. 17-2013-4030 E. 677493.1838 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2162.2m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION SC slightly moist **Asphalt CLAYEY SAND WITH GRAVEL**, occasional subrounded gravel, low to medium plasticity, brown note: calcareous, reacts with HCI SM S 11-8-5 SILTY SAND, some silt, trace clay, medium to slightly moist fine grained, well rounded sand, nonplastic, light brown moderately firm to soft note: calcareous, reacts with HCI Īυ 23  $\nabla$ S 1-1-3 5 6 S 4-6-10 ML 50/ SANDY SILT, trace clay, some to 8 140mm considerable fine grained sand, considerable slightly moist silt, medium plasticity, light purplish-brown hard note: highly calcareous, reacts with HCI Stopped Auger 7.6m Sampler refsued at 7.8m 10 Began HQ Coring at 7.8m 11 12 13 14 15 **GROUNDWATER** Page 1 of 2

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	4.3	14:45	10-19-13
$\bar{\blacksquare}$			

SAMPLE TYPE

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N613-B-1 U - 76mm O.D. 61mm I.D. tube sample. T - 25mm O.D. thin-walled tube sample



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 10-19-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 3976367.143 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 677493.1838 Sample Type % Core Recovery 2162.2m **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 3 Rock Type & Remarks Began HQ Coring at 7.8m 35 100 N/A 10/19 HQ N/A N/A N/A N/A SM/GM **CHINLE FORMATION** HQ 7.8 SILTSTONE, clayey in zones, calcareous, moderately 0 TL SIW soft to moderately hard, brown to reddish-brown Fld to L Cln with MdW 11.6 HQ 100 75 note: chemical reduction spots (1.6mm to 13mm) Slcks Mass ive zones note: bedding planes range from 0° to 15° at 8.5m note: abundant calcite nodules (white/gray) from 100 10/20 HQ 95 85 10.0m to 14.0m 15.8 1 6921 11 13.4 HQ 100 90 note: lenticular to cylindrical calcareous nodules about 13mm are abundant from 11.6m to 13.7m 12 note: healed fractures with brown (clayey & slight calcareous) infilling below 12.2m 13 note: clay & calcite fracture infilling along fracture 11.3 70 50 surfaces 13.0m 16986 note: occasional bedding planes dipping up to 45° below 13.4m MRgh curved Stopped HQ Coring at 14.0m note: low RQD values in zones due to mechanical breaks note: discontinuity spacing resultant from mechanical 15 breaks & relatively soft rock mass in some zones

	GROONDWATER			
	DEPTH (m)	HOUR	DATE	
$\nabla$	4.3	14:45	10-19-13	
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CDOLINDWATED

BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Navajo, New Mexico to N64 Junction, Arizona



3976371.754

**LOCATION DATE** 10/20/13 JOB NO. 17-2013-4030 E. 677508.1141 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2163.5m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 Graphical Log **DATUM** Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION SC slightly moist **Asphalt** CLAYEY SAND, trace fine grained, subangular gravel, low plasticity, brown note: calcareous, reacts with HCI SILTY SAND, predominantly fine grained SM S 2-4-8 sand, nonplastic, brown slightly moist 2 note: calcareous soft to moderately firm 3 S 2-2-3 4 ∏υ 8 5  $\nabla$ 6 S 1-1-8 note: medium grained sand S 8-10-SP-SM SAND WITH SILT, trace coarse grained 8 20 slightly moist gravel, nonplastic, brown × × × × × × × × note: does not react with HCI firm 9 SILTSTONE note: augered through weathered siltstone 10 to 9.8m Stopped Auger at 9.8m Began HQ Coring at 9.8m 11 12 13 14 15 **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	5.2	14:20	10-20-13
$ar{f A}$			

SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-21-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 3976371.754 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 677508.1141 Sample Type % Core Recovery 2163.5m **ELEVATION** Condition Depth in [ Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 8.8m 90 100 10/21 HQ 40 TL SIW CHINLE FORMANTION Rgh HQ part Fld SILTSTONE WITH ZONES OF SILTY SANDSTONE TO SANDY SILTSTONE, moderately hard to moderately soft, light gray to light greenish-gray, spotted purplish-red note: reduction spots 1.6mm to 6.4mm 15.2 HQ 90 60 10 note: some predominate high-angle healed fractures below 10.5m filled with brown clay/silt mixture 6040 note: purplish-brown from 10.7m to 13.1m -11 note: calcareous nodules below 10.7m up to 1.6mm in diameter 15.8 HQ 100 70 note: some partially calcite-filled fracture surfaces 12 13.4 13 HQ 15997 100 90 note: some calcite-healed fractures at 13.6m 14 Smth 12.4 100 HQ 100 15 Stopped HQ Coring at 14.9m note: low RQD values in zones due to mechanical breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones 16

	GROUNDWATER				
	DEPTH (m)	HOUR	DATE		
$\nabla$	5.2	14:20	10-20-13		
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CDOLINDWATED

**BORING OPERATION** 

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Navajo, New Mexico to N64 Junction, Arizona



3976285.707 **LOCATION** JOB NO. 17-2013-4030 **DATE** 10/22/13 E. 677486.7648 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2162.6m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM E Blows per 152 mr REMARKS VISUAL CLASSIFICATION GP slightly moist **Asphalt** SANDY GRAVEL, some medium to fine grained sand, predominantly subangular to SC subrounded gravel, dark gray note: does not react with HCI SM S 2-6-6 CLAYEY SAND, trace silt, predominantly fine slightly moist 2 grained sand, calcareous, low to medium plasticity, brown 3 note: calcareous, reacts with HCI 1797 Īυ 11 9 SILTY SAND, predominantly fine grained, slightly moist nonplastic, brown  $\nabla$ soft to note: not calcareous below 4.7m S 2-2-4 moderately firm 5 6 SC 1-1-2 **CLAYEY SAND**, predominantly fine grained sand, low to medium plasticity, brown wet note: occasional gravel very soft to firm note: does not react with HCI U 38 8 CL SANDY CLAY, some fine grained sand, S 2-2-4 considerable clay, slightly calcareous, medium moist plasticity, reddish-gray 10 soft note: does not react with HCI S 2-3-4 11 12 **SILTY SAND**, occasional fine grained gravel, predominantly fine to medium grained, SM U wet nonplastic, brown 13 soft to firm note: reacts to HCI S 4-9-10 14 15 3-8-11 note: cemented/flaky **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\nabla}$	4.4		10-22-13
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 3

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample. LOG OF TEST BORING NO.N613-B-3

PROJECT_	BIA Project N12 (12-2) (19-2) 2 & 4
	Navajo, New Mexico to N64 Junction, Arizona



									LOCATION _	N.	3976285.707
JOB NO	D17	7-2013-4	030	)	_ DATE	10/22	2/13		_	E.	677486.7648
									RIG TYPE		CME-85 Buggy Mounted
									BORING TYPE		203mm Hollow Stem Auger
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ω	٤	ica	<u>e</u>	le T	no	ensi r met	eig of	d Sc fica	DATUM		GPS NAD 83 - UTM Zone 12
Depth in Meters	Blows per 152 mm	Graphical Log	Sample	Sample Type	Blow Counts	Dry Density Kg. per Cubic meter	Moisture Content Percent of Dry Weight	Unified Soil Classification	REMARKS		VISUAL CLASSIFICATION
16											SILTY SAND, continued
											Stopped Auger at 16.2m Began HQ Coring at 16.2m
											Began HQ Coring at 16.2m
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	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	4.4		10-22-13
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SAMPLE TYPE

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample.
T - 25mm O.D. thin-walled tube sample



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-23-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling Boring Operation and Drill Rate (min/meter) Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Rock Quality Designation (RQD) Spacing Orientation **N.** 3976285.707 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric **E.** 677486.7648 Sample Type % Core Recovery 2162.6m **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 2 5 3 4 Rock Type & Remarks Began HQ Coring at 16.2m 16 HQ 50 100 **BROKEN** 10/23 0 N/A Mass-MdW CHINLE FORMANTION HQ 6.2 ive CALCAREOUS SILTSTONE, soft, reddish-brown with occasional green spots note: greenish-gray to gray reduction spots 17 note: considerable clay content throughout note: lamination = <0.8mm to 1.6mm 9.0 HQ 80 10 18 MRgh TL Cln in BROKEN note: healed fracture filled with clay at 18.6m zones 19 note: soft with very soft zones below 18.7m 8.8 SIW HQ 90 85 MdW 6049 -20 11.3 HQ 100 85 -21 note: decrease in reduction spots below 21.8m 22 Stopped HQ Coring at 22.3m note: low RQD values in zones due to mechanical breaks & soft rockmass -23 note: discontinuity spacing resultant from mechanical breaks & relatively soft rockmass in some zones

	GROUNDWATER							
	DEPTH (m)	HOUR	DATE					
$\nabla$	4.4		10-22-13					
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**BORING OPERATION** 

D - Disturbed Bulk Sample

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

Page 3 of 3



3976286.21 **LOCATION** JOB NO. 17-2013-4030 **DATE** 10/21/13 E. 677497.3724 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2158.9m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log Blows per 152 mm Sample **REMARKS** VISUAL CLASSIFICATION SM slightly moist **Asphalt** SILTY SAND, trace subrounded gravel, predominantly fine grained sand, nonplastic, very soft to soft pinkish-brown note: calcareous, reacts with HCI 6-6-8 2 3 1763 Īυ 16 13  $\nabla$ s 1-1-1 5 6 U SP-SM SAND WITH SILT, predominantly medium S 2-2-4 8 grained sand, nonplastic, brown wet note: does not react with HCI soft 9 CL SANDY CLAY, predominantly fine grained 3-3-6 sand, medium to high plasticity, dark gray & moist brown 10 stiff note: does not react with HCI 25-30-ML SANDY SILT, trace medium to coarse grained 11 slightly moist sand, some fine grained sand, calcareous, pinkish-brown hard note: calcareous, reacts with HCL 12 Stopped Auger at 10.7m Stopped Sampler at 11.1m 13 Began HQ Coring at 11.1m 14 15 GROUNDWATER

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$	4.4		10-21-13
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery
S - 51mm O.D. 35mm I.D. tube sample.
U - 76mm O.D. 61mm I.D. tube sample. LOG OF TEST BORING NO.N613-B-4



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 10-21-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 3976286.21 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 677497.3724 Sample Type 2158.9m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 3 Rock Type & Remarks Began HQ Coring at 10.7m 10/21 HQ 65 95 0 Mass-HiW CHINLE FORMANTION Smth HQ 3.3 ive SILTSTONE, clayey in zones, soft to moderately soft, SRgh 11 reddish-brown with green spots Stn note: greenish-gray to gray reduction spots up to 13mm in diameter, calcareous, some clear nodules 0.8mm to 12.4 HQ 100 90 25 BROKEN 1.6mm MdW 12 note: clayey from 10.7m to 11.9m to SIW SILTSTONE, calcareous in parts, dark brown with greenish-gray nodules note: moderately soft to moderately hard below 11.9m 18325 note: numerous predominantly high-angle healed 10/22 HQ 100 55 some 13.2 fractures, clay filled (6mm), dark brown curved Fld Rgh 14 note: increase in predominantly high-angle clay-healed **BROKEN** fractures below 14.6m 13.2 HQ 100 35 Rgh Fld note: some iron-oxide staining on fracture surfaces 15 at 15.1m 12018 SRgh clay Fld 16 12.5 100 HQ 90 Slcks w/step like note: some calcareous infilling features Stopped HQ Coring at 16.8m 17 note: low RQD values in zones due to mechanical breaks & soft rockmass note: discontinuity spacing resultant from mechanical breaks & relatively soft rockmass in some zones 18

	GROUNDWATER							
	DEPTH (m)	HOUR	DATE					
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CDOLINDWATED

BORING OPERATION

D - Disturbed Bulk Sample

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

Navajo, New Mexico to N64 Junction, Arizona



3991204.956 **LOCATION** JOB NO. 17-2013-4030 **DATE** 10/24/13 676150.9859 E. CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2218.8m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log m Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION SC slightly moist 152mm Asphalt CLAYEY SAND & GRAVEL, considerable subrounded gravel, calcareous, low plasticity note: reacts to HCI U 1901 12 33 S 4-10-SM SILTY SAND, predominantly fine grained sand, moderately calcareous, yellow to tan 10 moist grading to black 4 firm note: reacts to HCI S 2-2-3 CL-ML note: increased clay, low plasticity 5 SANDY SILTY CLAY, considerable predominantly fine grained sand, low plasticity, moist 6 7 15 SM soft note: does not react with HCI SILTY SAND, predominantly fine grained moist sand, nonplastic, gray moderately firm note: does not react with HCI SP-SM S 3-3-6 SAND WITH SILT, considerable 8 wet predominantly fine to medium grained, subrounded sand, nonplastic, tan stiff 9 note: does not react with HCI SM 2-2-3 SILTY SAND, predominantly fine to medium grained, subrounded sand, some subrounded wet gravel, brown 10 soft note: does not react with HCI S 6-8-12 SP-SM SAND WITH SILT, occasional subrounded 11 gravel, trace silt, medium grained, subrounded wet sand, brown very stiff note: does not react with HCI 12 Stopped Auger at 11.6m Began HQ Coring at 11.6m 13 14 15 **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$		none	
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SAMPLE TYPE

A - Auger cuttings; NR-No Recovery

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N614-B-1 U - 76mm O.D. 61mm I.D. tube sample.



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-26-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 3991204.956 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 676150.9859 Sample Type % Core Recovery 2218.8m **ELEVATION** Condition Depth in [ Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 11.6m HQ 90 100 MdW 10/26 35 Rgh Cln TL CHINLE FORMANTION HQ 7.4 SILTSTONE/CLAYSTONE, calcareous in zones, moderately soft to soft, reddish-brown 12 note: grayish-green chemical reduction (0.8mm to 1.6mm) note: clayey in zones 10.8 75 25 HQ 13 note: calcareous nodules from 11.9m to 12.8m 7445 14 HQ 55 25 note: moderately soft to moderately hard sandy siltstone, abundant calcite, clayey zones dark red to brown from 14.3m to 16.2m -15 note: dark green spots 1.5mm to 3.0mm from 15.5m to 15.8m 8.6 HQ 85 60 16 SIW note: moderately hard below 16.2m 17 18795 9.0 HQ 100 80 Stopped HQ Coring at 17.7m note: low RQD values in zones due to mechanical 18 breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones note: water used while coring, therefore unknown if groundwater encountered

	GROUNDWATER							
	DEPTH (m)	HOUR	DATE					
$\nabla$		none						
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$\bar{\mathbf{A}}$								
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BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample



3991202.526

N.

**LOCATION** JOB NO. 17-2013-4030 **DATE** 10/26/13 E. 676158.2223 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2218.9m SURFACE ELEV. Unified Soil Classification Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 DATUM Graphical Log Sample E **REMARKS** VISUAL CLASSIFICATION SC slightly moist 152mm Asphalt CLAYEY SAND & GRAVEL, some clay, considerable subangular gravel, predominantly moderately firm fine grained sand, calcareous, low to medium plasticity, pinkish-brown S 4-6-7 note: decrease in gravel at 2.0m note: reacts to HCI 3 S 6-12-15 4 1819 U 15 16 5 SM SILTY SAND, trace clay, considerable predominantly fine grained sand, highly calcareous, nonplastic, tan moist 6 S 2-3-6 note: grayish-tan moderately firm note: hair roots note: reacts to HCI U 18 8 SP-SM SAND WITH SILT, predominantly fine to S 3-4-6 medium grained sand, nonplastic, tan wet 10 note: does not react with HCI stiff 47 CL-ML SANDY SILTY CLAY, low to medium U 11 plasticity, pinkish-reddish-brown moist note: does not react with HCI hard 12 Stopped Auger at 10.7m Stopped Sampler at 11.0m Began HQ Coring at 10.7m 13 14 15 **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$		none	
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SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

Page 1 of 2

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N614-B-2 U - 76mm O.D. 61mm I.D. tube sample.



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 10-27-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 3991202.526 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 676158.2223 Sample Type % Core Recovery 2218.9m **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 10.7m 0 100 NO RECOVERY NO RECOVERY MdW 10/27 HQ None TL CHINLE FORMANTION HQ 3.7 SILTSTONE/CLAYSTONE, moderately soft to moderately hard, calcareous, reddish-brown note: grayish-green chemical reduction spots (0.8mm to 13mm) 7.6 HQ 95 10 note: abundant grayish-green clay seams, moderately 12 soft to soft note: soft brecciated & green zone from 13.7m to 13.8m Rgh Stn HiW 13 7.6 HQ 10887 15 BROKEN Smth Stn 14 note: some calcite-filled fracture surfaces at 14.5m 7.4 HQ 80 40 note: sandy siltstone, calcareous, moderately hard to 15 moderately soft from 14.6m to 16.2m SRgh Gouge note: thin gouge zone from 15.1m to 15.2m -16 5.0 HQ 14321 60 20 **BROKEN** Stopped HQ Coring at 16.8m 17 note: low RQD values in zones due to mechanical breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones note: water used while coring, therefore unknown if groundwater encountered 18

	GROUNDWATER							
	DEPTH (m)	HOUR	DATE					
$\nabla$								
T								
$\bar{\mathbf{A}}$								

BORING OPERATION

D - Disturbed Bulk Sample

B - BDBGM 51mm O.D. Wireline Rock Coring BWC - B-size casing

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

Navajo, New Mexico to N64 Junction, Arizona



3991161.265 **LOCATION** JOB NO. 17-2013-4030 **DATE** 10/24/13 E. 676147.8781 CME-85 Buggy Mounted **RIG TYPE** 203mm Hollow Stem Auger **BORING TYPE** 2218.0m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log ШШ Sample Blows per 152 mr REMARKS VISUAL CLASSIFICATION SC slightly moist 152mm Asphalt CLAYEY SAND WITH GRAVEL, considerable gravel, 10% rare crystalline red & green mottled moderately firm limestone cobbles, low to medium plasticity, light pinkish-brown GC S 10-9-6 note: does not react with HCI note: unweathered core stones of same composition **CLAYEY GRAVEL WITH SAND.** considerable CL S 17-9fine to coarse grained sand, fine to coarse 8 grained gravel, medium plasticity, light brown SANDY CLAY, occasional gravel, trace silt, 4 slightly moist highly calcareous, medium plasticity, brownish-pink firm U 39 5 note: reacts to HCI 6 SM S 5-5-26 SILTY SAND, nonplastic, light brown moist note: reddish-brown, increase in clay at 6.9m very firm to hard note: does not react with HCI 50/ Stopped Auger at 7.6m 8 76mm Sampler refused at 7.7m Began HQ Coring at 7.7m 9 10 11 12 13 14 15 **GROUNDWATER** 

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$		none	
Ī			

SAMPLE TYPE

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N614-B-3 U - 76mm O.D. 61mm I.D. tube sample. T - 25mm O.D. thin-walled tube sample

Page 1 of 2



CME-85 Buggy Mounted **RIG TYPE JOB NO.** 17-2013-4030 10-24-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling <u>=</u> Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Boring Operation and Rate (min/meter) Rock Quality Designation (RQD) Spacing Orientation **N.** 3991161.265 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 676147.8781 Sample Type 2218.0m % Core Recovery **ELEVATION** Condition Depth in Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 7.6m HQ 10 100 MRgh 10/24 0 TL MdW CHINLE FORMANTION HQ 5.0 Stn SILTSTONE/CLAYSTONE, calcareous, moderately soft to moderately hard, clayey in parts, purplish-brown note: purplish-brown & brown reduction spots (green) dispersed throughout 10.5 HQ 80 10 BROKEN note: green reduction zones healed fractures at 9m **BROKEN** 12149 10 SRgh Fld 9.5 HQ 90 30 note: some variably-oriented calcite healed fractures at 10.2m SIW Smth MdW 11 12.6 HQ 85 10 15093 12 Smth BROKEN note: alternating green, softer zones up to 51mm to 76mm thick at 12.2m SIW 6.7 HQ 85 0 13 slcks 15.0 100 HQ 65 Stopped HQ Coring at 13.7m note: low to zero RQD values in zones due to 14 mechanical breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones note: water used while coring, therefore unknown if groundwater encountered 15

	GROUNDWATER							
	DEPTH (m)	HOUR	DATE					
$\nabla$		none						
▼								
<u>A</u>								

CDOLINDWATED

BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample

Navajo, New Mexico to N64 Junction, Arizona



3991162.872

**LOCATION DATE** 10/24/13 JOB NO. 17-2013-4030 E. 676153.8745 CME-85 Buggy Mounted RIG TYPE 203mm Hollow Stem Auger **BORING TYPE** 2220.3m Unified Soil Classification SURFACE ELEV. Sample Type Blow Counts Dry Density Kg. per Cubic meter Moisture Content Percent of Dry Weight GPS NAD 83 - UTM Zone 12 **DATUM** Graphical Log шш Sample Blows per 152 mr **REMARKS** VISUAL CLASSIFICATION SC slightly moist 152mm Asphalt **CLAYEY SAND WITH GRAVEL**, trace silt, some fine grained gravel, predominantly fine moderately firm grained sand, low to medium plasticity, reddish-brown S 5-6-6 note: does not react with HCI Īυ 16 4 S 6-12note: increase clay, decrease silt, increase 5 13 medium grained sand, medium plasticity at 4.6m 6 S 6-12-24 SC-SM SILTY CLAYEY SAND WITH GRAVEL, some S 12-24-8 fine grained gravel, predominantly medium 36 slightly moist grained sand, low to medium plasticity, reddish-brown, calcareous hard note: reacts to HCI S 29-50/ SM SILTY SAND WITH GRAVEL, considerable 127mm slightly moist fine grained gravel, calcareous, nonplastic, 10 reddish-brown hard note: reacts to HCI 11 Stopped Auger at 9.1m Sampler refused at 9.4m Began HQ Coring at 9.4m 12 13 14 15 **GROUNDWATER** Page 1 of 2

	DEPTH (m)	HOUR	DATE
$\bar{\Delta}$		none	
Ā			

SAMPLE TYPE

T - 25mm O.D. thin-walled tube sample

A - Auger cuttings; NR-No Recovery S - 51mm O.D. 35mm I.D. tube sample. LOG OF TEST BORING NO.N614-B-4 U - 76mm O.D. 61mm I.D. tube sample.



CME-85 Buggy Mounted **JOB NO.** \_ 17-2013-4030 **RIG TYPE** 10-26-13 DATE **HQ** Wireline METHOD **DISCONTINUITIES OPERATOR** CasCade Drilling Boring Operation and Drill Rate (min/meter) Unconfined Compression of Point Load index Test (KPa) Reed Seamons LOGGED BY Rock Quality Designation (RQD) Spacing Orientation **N.** 3991162.872 LOCATION Weathering or USCS (Soils) Meter % Drilling Fluid/Air Rec. Bedding and/ or Fabric E. 676153.8745 Sample Type 2220.3m % Core Recovery **ELEVATION** Condition Depth in [ Wide - Close Horiz-Vert Sample DATUM GPS NAD 83 - UTM Zone 12 Vertical INCLINATION 5 Rock Type & Remarks Began HQ Coring at 9.1m 9 HQ 40 100 10/26 10 Smth TL SIW CHINLE FORMANTION HQ 4.3 Slcks to SILTSTONE/CLAYSTONE, calcareous in parts, MdW moderately soft to moderately hard, clayey in parts, reddish-brown 10 note: grayish-green reduction spots up to 0.8mm to 12.2 HQ 75 60 1.6mm note: mechanical fractures along bedding plans dipping from 5° to 15° 11 7.2 HQ 90 30 12 Slcks Smth Fld 13 **BROKEN** Smth Gouge 7.8 HQ 100 30 TL note: thin gouge zone from 13.0m to 13.1m Stn 9758 ] -14 1 Smth SRgh Stn 6.5 HQ 90 60 -15 Stopped HQ Coring at 15.2m note: low to zero RQD values in zones due to mechanical breaks note: discontinuity spacing resultant from mechanical breaks & relatively soft rock mass in some zones 16 note: water used while coring, therefore unknown if groundwater encountered

GROUNDWATER					
	DEPTH (m)	HOUR	DATE		
$\nabla$		none			
▼					
<u>A</u>					

CDOLINDWATED

BORING OPERATION

B - BDBGM 51mm O.D. Wireline Rock Coring

BWC - B-size casing HQ - 96mm O.D. Wireline Rock Coring NQ - 71mm O.D. Wireline Rock Coring S - 51mm O.D./35mm I.D. Tube Sample

D - Disturbed Bulk Sample



**APPENDIX B** 

**CORE PHOTOS** 

## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 1
Bridge N503, Boring No. 1, 8.84 meters to 12.04 meters



Photograph No. 2
Bridge N503, Boring No. 1, 12.04 meters to 14.63 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 3
Bridge N503, Boring No. 1, 14.63 meters to 15.39 meters



**Photograph No. 4**Bridge N503, Boring No. 2, 11.89 meters to 14.63 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 5
Bridge N503, Boring No. 2, 14.63 meters to 17.47 meters



Photograph No. 6
Bridge N503, Boring No. 2, 17.47 meters to 18.29 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 7
Bridge N503, Boring No. 3, 10.67 meters to 15.58 meters



**Photograph No. 8**Bridge N503, Boring No. 3, 15.58 meters to 16.76 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



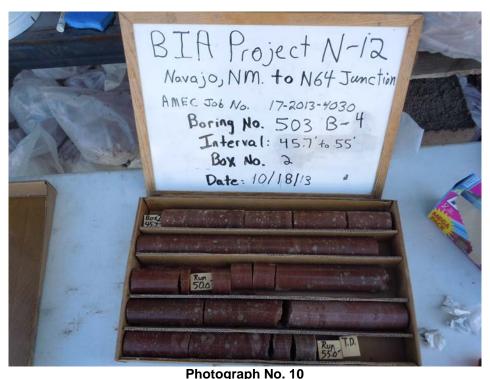
## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 9
Bridge N503, Boring No. 4, 10.51 meters to 13.93 meters



Bridge N503, Boring No. 4, 13.93 meters to 16.76 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



**Photograph No. 11**Bridge N505, Boring No. 1, 4.27 meters to 7.86 meters



Bridge N505, Boring No. 1, 7.86 meters to 10.67 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 13
Bridge N505, Boring No. 2, 4.42 meters to 12.34 meters



Bridge N505, Boring No. 2, 12.34 meters to 15.24 meters

AMEC Job No. 17-2013-4030

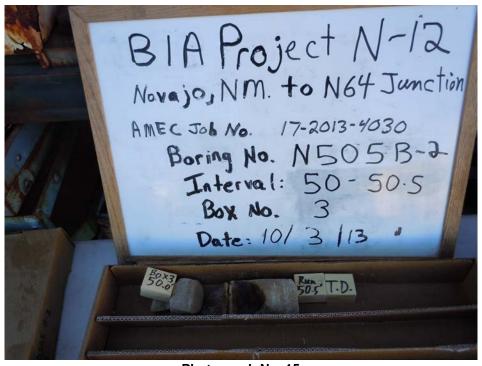
Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 15
Bridge N505, Boring No. 2, 15.24 meters to 15.39 meters



**Photograph No. 16**Bridge N505, Boring No. 3, 4.42 meters to 7.83 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE) Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek;

# N614, Coyote Wash; N613, Tohdildonih Wash PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 17
Bridge N505, Boring No. 3, 7.83 meters to 10.64 meters



**Photograph No. 18**Bridge N505, Boring No. 3, 10.64 meters to 11.13 meters

AMEC Job No. 17-2013-4030 Photographed By: Alex Yiannakakis



### NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



**Photograph No. 19**Bridge N505, Boring No. 4, 2.74 meters to 6.25 meters



Bridge N505, Boring No. 4, 6.25 meters to 9.02 meters

AMEC Job No. 17-2013-4030

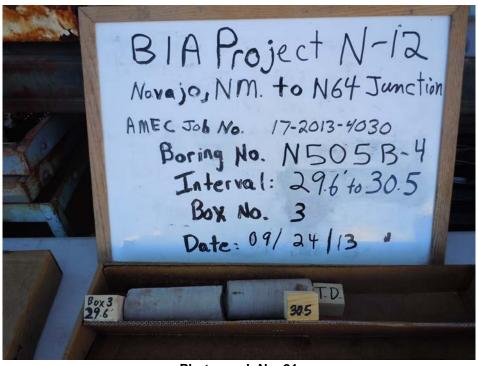
Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 21
Bridge N505, Boring No. 4, 9.02 meters to 9.30 meters



Photograph No. 22
Bridge N613, Boring No. 1, 7.92 meters to 11.16 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



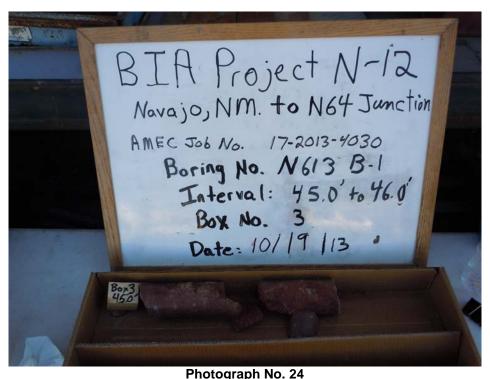
## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 23
Bridge N613, Boring No. 1, 11.16 meters to 13.72 meters



Bridge N613, Boring No. 1, 13.72 meters to 14.02 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 25
Bridge N613, Boring No. 2, 8.84 meters to 11.64 meters



Photograph No. 27
Bridge N613, Boring No. 2, 11.64 meters to 14.23 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 27
Bridge N613, Boring No. 2, 14.23 meters to 14.94 meters



Bridge N613, Boring No. 3, 16.15 meters to 19.57 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Bridge N613, Boring No. 3, 19.57 meters to 22.25 meters



Bridge N613, Boring No. 4, 10.67 meters to 13.53 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 31
Bridge N613, Boring No. 4, 13.53 meters to 16.15 meters



Bridge N613, Boring No. 4, 16.15 meters to 16.76 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



#### NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 33
Bridge N614, Boring No. 1, 11.58 meters to 14.63 meters



**Photograph No. 34**Bridge N614, Boring No. 1, 14.63 meters to 17.68 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 35
Bridge N614, Boring No. 2, 10.67 meters to 13.90 meters



**Photograph No. 36**A Bridge N614, Boring No. 2, 13.90 meters to 16.76 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



### NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 37
Bridge N614, Boring No. 3, 7.62 meters to 11.43 meters



Bridge N614, Boring No. 3, 11.43 meters to 13.72 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis



## NAVAJO, NEW MEXICO TO N64 JUNCTION, ARIZONA (NEAR TSAILE)

Bridge Sites: N505, Tsaile Creek; N504, Wheatfield Creek; N503, Whiskey Creek; N614, Coyote Wash; N613, Tohdildonih Wash

#### PHOTOGRAPHIC LOG OF ROCK CORE



Photograph No. 39
Bridge N614, Boring No. 4, 9.14 meters to 12.37 meters



Bridge N614, Boring No. 4, 12.37 meters to 15.24 meters

AMEC Job No. 17-2013-4030

Photographed By: Alex Yiannakakis





# APPENDIX C LABORATORY TEST RESULTS



#### LABORATORY TESTING PROCEDURES

Consolidation Tests Soiltest or Clockhouse apparatus of the "floating-ring" type are employed for the one-dimensional consolidation tests. They are designed to receive 1-inch high 2.5-inch O.D. brass liner rings with soil specimens as secured in the field. Procedures for the tests generally are those outlined in ASTM D2435. Loads are applied in several increments to the upper surface of the test specimen and the resulting deformations are recorded at selected time intervals for each increment. For soils which are essentially saturated, each increment of load is maintained until the deformation versus log of time curve indicates completion of primary consolidation. For partially saturated soils, each increment of load is maintained until the rate of deformation is equal or less than 1/10,000 inch per hour. Applied loads are such that each new increment is equal to the total previously applied loading. Porous stones are placed in contact with the top and bottom of the specimens to permit free addition or expulsion of water. For partially saturated soils, the tests are normally performed at in situ moisture conditions until consolidation is complete under stresses approximately equal to those which will be imposed by the combined overburden and foundation loads. The samples are then submerged to show the effect of moisture increase and the tests continued under higher loadings. Generally, the tests are continued to about twice the anticipated curve due to overburden and structural loads with a rebound curve then being established by releasing loads.

**Expansion Tests** The same type of consolidometer apparatus described above is used in expansion testing. Undisturbed samples contained in brass liner rings are placed in the consolidometers, subjected to appropriate surcharge loads and submerged. The loads are maintained until the expansion versus log of time curve indicates the completion of "primary swell".

<u>Direct Shear Tests</u> Direct shear tests are run using a Clockhouse or Soiltest apparatus of the strain-control of approximately 0.05 inch per minute. The machine is designed to receive one of the 1-inch high 2.42-inch diameter specimens obtained by tube sampling. Generally, each sample is sheared under a normal load equivalent to the effective overburden pressure at the point of sampling. In some instances, samples are sheared at several normal loads to obtain the cohesion and angle of internal friction. When necessary, samples are saturated and/or consolidated before shearing in order to approximate the anticipated controlling field loading conditions.

			SUMMARY OF	TABLE C-		SULTS				
Boring Number	(meters)	Depth	USCS/Group Symbol or Rock Type	Percent Fines (minus 200)	Liquid Limit	Plasticity Index	Direct Shear Peformed	Collapse (%)¹ [Swell (+) / Collapse (-)]	Unconfined Compressive Strength of Soil (Kpa) <sup>2</sup>	Unconfined Compressive Strength of Rock (Kpa) <sup>2</sup>
ēr	Begin	End	nbol or	ŭ	_	ex	ormed	)¹ )se (-)]	ressive (Kpa)²	ressive (Kpa)²
N503 B-1	0.00	1.52	SC-SM	30	21	7				
N503 B-1	2.44	2.90	CL	51	30	11				
N503 B-1	3.81	4.27	<sup>3</sup> CL-ML	07	ND /	ND	✓			
N503 B-1 N503 B-1	5.49 7.01	5.94 7.47	ML GM	67 18	NV NV	NP NP		1		
N503 B-1	10.52	10.67	<sup>3</sup> Siltstone	10	INV	NP NP				25,249
N503 B-1	13.72	13.94	<sup>3</sup> Siltstone							30,100
N503 B-2	1.52	1.98	CL-ML	63	26	7				00,100
N503 B-2	3.05	3.51	CL	52	30	8				
N503 B-2	4.57	4.88	<sup>3</sup> CL					-1.2		
N503 B-2	6.10	6.40	GM	13	NV	NP				
N503 B-2	7.62	7.92	<sup>3</sup> SM				✓			
N503 B-2	15.39	15.58	<sup>3</sup> Siltstone							12,844
N503 B-3	0.00	1.52	CL-ML	50	22	6				
N503 B-3 N503 B-3	3.05 4.57	3.51 4.88	ML <sup>3</sup> ML	51	19	3			18	
N503 B-3 N503 B-3	6.10	6.55	GP-GM	11	NV	NP			10	
N503 B-3	7.62	8.08	SP-SM	9.1	NV	NP				
N503 B-3	9.14	9.45	SM	12	NV	NP				
N503 B-3	10.67	10.97	SC-SM	22	23	6				
N503 B-3	12.53	12.65	<sup>3</sup> Siltstone							18,623
N503 B-3	16.49	16.64	<sup>3</sup> Siltstone							40,142
N503 B-4	1.52	1.98	SM	41	NV	NP				
N503 B-4	3.05	3.35	<sup>3</sup> SM					-0.3		
N503 B-4	4.57	5.03	GM	16	NV NV	NP				
N503 B-4	6.10	6.55	SM	40	NV NV	NP ND				
N503 B-4 N503 B-4	7.62 9.14	8.08 9.45	SP <sup>3</sup> SM	1.6	NV	NP	<b>✓</b>			
N503 B-4	13.38	13.53	<sup>3</sup> Siltstone				+ -			31,202
N503 B-4	15.79	15.85	<sup>3</sup> Siltstone							32,531
N504 B-1	0.00	1.52	SM	27	NV	NP				02,00
N504 B-1	2.44	2.74	<sup>3</sup> SM					0		
N504 B-1	4.57	5.03	SM	30	18	2				
N504 B-1	12.19	12.50	CL	92	40	20				
N504 B-1	13.72	14.02	CL	89	37	23				
N504 B-1	15.24	15.48	CL 3 c.	72	42	25	<b>_</b>			
N504 B-1 N504 B-2	16.76	17.07	³CL				✓ ✓			
N504 B-2 N504 B-2	3.20 4.57	3.35 5.03	<sup>3</sup> SM SM	25	NV	NP	<b>- v</b>			
N504 B-2	9.30	9.60	<sup>3</sup> SM	20	14.0	141	+		41	
N504 B-3	0.00	1.52	SC	37	30	16	†		,,	
N504 B-3	3.05	3.51	SC	45	35	22	1			
N504 B-3	7.01	7.32	<sup>3</sup> SM				✓	<u> </u>		
N504 B-3	14.48	14.78	<sup>3</sup> ML						6	
N504 B-4	1.52	1.98	CL	58	37	23				
N504 B-4	4.72	5.03	<sup>3</sup> SM				<del>                                     </del>	-0.2		
N504 B-4	7.62	8.08	SP-SM	7.6	NV	NP				
N505 B-1	1.52	1.83	³SC	40	0.5	40	✓			
N505 B-1	3.05 6.54	3.20 6.71	GC	19	25	12	1			12 722
N505 B-1 N505 B-1	10.36	10.55	<sup>3</sup> Sandstone <sup>3</sup> Sandstone				+			43,733 40,539
N505 B-1	1.52	1.98	SC	39	26	13	+			70,008

			SUMMARY OF L	TABLE C		SULTS				
Boring Number	(meters)	Depth	USCS/Group Symbol or Rock Type	Percent Fines (minus 200)	Liquid Limit	Plasticity Index	Direct Shear Peformed	Collapse (%)¹ [Swell (+) / Collapse (-)]	Unconfined Compressive Strength of Soil (Kpa) <sup>2</sup>	Unconfined Compressive Strength of Rock (Kpa) <sup>2</sup>
Jer -	Begin	End	nbol or	) es	7	ex	ormed	) <sup>1</sup> pse (-)]	oressive (Kpa) <sup>2</sup>	oressive (Kpa) <sup>2</sup>
N505 B-2	2.29	2.59	<sup>3</sup> SC				✓			
N505 B-2	3.81	3.96	SC	43	34	14				00.004
N505 B-2 N505 B-2	11.70 13.38	11.90 13.53	<sup>3</sup> Sandstone							39,061 33,827
N505 B-2	1.22	1.68	<sup>3</sup> Sandstone CL	75	36	20				33,021
N505 B-3	6.22	6.43	<sup>3</sup> Sandstone	70	00	20				42,314
N505 B-3	10.47	10.61	<sup>3</sup> Sandstone							24,694
N505 B-4	0.00	1.52	CL	54	29	14				
N505 B-4	1.52	1.83	<sup>3</sup> SM				✓			
N505 B-4	9.02	9.17	<sup>3</sup> Sandstone		,		1			37,604
N613 B-1	1.52	1.98	SM	30	NV	NP				
N613 B-1 N613 B-1	3.05 4.57	3.35 5.03	<sup>3</sup> SM SM	30	NV	NP	<b>✓</b>			
N613 B-1	6.10	6.25	SM	20	NV	NP NP				
N613 B-1	10.45	10.61	<sup>3</sup> Siltstone	20	INV	INI				6,921
N613 B-1	13.20	13.35	<sup>3</sup> Siltstone							16,986
N613 B-2	0.00	1.52	SC	48	28	14				-,
N613 B-2	3.05	3.51	SM	31	NV	NP				
N613 B-2	6.10	6.55	SM	37	NV	NP				
N613 B-2	7.62	8.08	SP-SM	8.8	NV	NP				
N613 B-2	10.70	10.82	<sup>3</sup> Siltstone							6,040
N613 B-2 N613 B-3	12.98 1.52	13.20 1.98	<sup>3</sup> Siltstone SM	27	NV	NP				15,997
N613 B-3	3.05	3.35	<sup>3</sup> SM	21	INV	INF		-0.1		
N613 B-3	4.57	5.03	SM	17	NV	NP		-0.1		
N613 B-3	6.10	6.55	SC	37	27	9				
N613 B-3	7.62	7.92	<sup>3</sup> SC	-			✓			
N613 B-3	9.14	9.60	CL	75	44	27				
N613 B-3	10.67	11.13	CL	77	37	23				
N613 B-3	12.19	12.50	<sup>3</sup> SM				✓			
N613 B-3	13.72	14.17	SM	33	NV	NP				
N613 B-3	15.24	15.70 19.93	SM	34	NV	NP				6.049
N613 B-3 N613 B-4	19.78 1.52	1.98	<sup>3</sup> Siltstone SM	36	NV	NP				0,049
N613 B-4	3.05	3.35	<sup>3</sup> SM	30	INV	INI		-0.1		
N613 B-4	6.10	6.40	<sup>3</sup> SM				<b>√</b>	0.1		
N613 B-4	7.62	8.08	SP-SM	5.3	NV	NP				
N613 B-4	9.14	9.60	CL	70	46	32				
N613 B-4	10.67	11.13	ML	71	NV	NP				
N613 B-4	12.86	13.01	<sup>3</sup> Siltstone				<del>                                     </del>			18,325
N613 B-4	15.15	15.32	<sup>3</sup> Siltstone				<del> </del>	0.1		12,018
N614 B-1 N614 B-1	1.68 3.05	1.98 3.51	<sup>3</sup> SC SM	39	NV	NP	<del>                                     </del>	-0.1		
N614 B-1	4.57	5.03	CL-ML	59 	24	7	+			
N614 B-1	6.25	6.55	<sup>3</sup> SM			,	<b>✓</b>			
N614 B-1	7.62	8.08	SP-SM	5.6	NV	NP				
N614 B-1	9.14	9.60	SM	13	NV	NP				
N614 B-1	10.67	11.13	SP-SM	5.6	NV	NP				
N614 B-1	13.90	14.02	<sup>3</sup> Siltstone/Claystone							7,445
N614 B-1	17.10	17.22	<sup>3</sup> Siltstone/Claystone				1			18,795
N614 B-2	3.05	3.51	SC 300	38	28	12	1	0.7		
N614 B-2	4.57	4.88	<sup>3</sup> SC		L	J		-0.7	<u> </u>	

			0	TABLE C						
			SUMMARY OF L	ABORATO	RY TEST RE	SULTS	ı	ı	_	_
Boring Number	(meters)	Depth	USCS/Group Symbol or Rock Type	Percent Fines (minus 200)	Liquid Limit	Plasticity Index	Direct Shear Peformed	Collapse (%)¹ [Swell (+) / Collapse (-)]	Unconfined Compressive Strength of Soil (Kpa) <sup>2</sup>	Unconfined Compressive Strength of Rock (Kpa)²
nber	Begin	End	ymbol or oe	nes )0)	nit	ndex	eformed	%)¹ apse (-)]	npressive il (Kpa)²	npressive ck (Kpa)²
N614 B-2	6.10	6.55	SM	34	NV	NP				
N614 B-2	9.14	9.60	SP-SM	6.3	NV	NP				
N614 B-2	10.67	10.97	<sup>3</sup> CL-ML				✓			
N614 B-2	13.11	13.26	<sup>3</sup> Siltstone/Claystone							10,887
N614 B-2	16.22	16.34	<sup>3</sup> Siltstone/Claystone							14,321
N614 B-3	0.00	1.52	SC	32	27	13				
N614 B-3	1.52	1.98	GC	33	30	15				
N614 B-3	3.05	3.51	CL	53	32	16				
N614 B-3	6.10	6.55	SM	41	NV	NP				
N614 B-3	9.85	10.00	<sup>3</sup> Siltstone/Claystone							12,149
N614 B-3	11.89	12.01	<sup>3</sup> Siltstone/Claystone							15,093
N614 B-4	1.52	1.98	SC	36	29	13				
N614 B-4	3.05	3.35	3SC				✓			
N614 B-4	4.57	5.03	SC	26	41	24				
N614 B-4	6.10	6.55	SC	43	28	11				
N614 B-4	7.62	8.08	SC-SM	38	25	7				
N614 B-4	9.14	9.45	SM	23	NV	NP				
N614 B-4	13.44	13.66	<sup>3</sup> Siltstone/Claystone							9,758
			Average	36.8				-0.3	21.7	22,259
			Standard Deviation	21.5				0.4	17.8	12,494
			Maximum	92				0	41	43,733
			Minimum	2		07	40	-1.2	6.0	6,040
			Count	67	67	67	16	8	3	28



BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

1720134030.0002

WORK ORDER NO:

3

DATE ASSIGNED:

10/2/13

Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00)
Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05)
GROUP SYMBOL, USCS (ASTM D-2487)

#### SIEVE SIZES

	Silt or								SAND								GRAVE	L				COBBLES	1
	Clay Fine					Mediun	1	Co	arse		Fi	ne				Coarse	**************************************	-	CODDELO				
Location & Depth	USCS	LL	PI	75um	150um	300um	425um	600um	1.18um	2.00mm	2.36mm	4.75mm	6.3mm	9.5mm	12.5mm	19mm	25mm	31.2mm	37.5mm	50mm	75mm	152mm	Lab#

#### PERCENT PASSING BY WEIGHT

	N504 B-1; 4.57 m - 5.03 m	SM	18	2	30	54	84	95	98	99	100	100	100	100	100	100	100	100	100	100	100	100	100	247
-	N504 B-1; 12.19 m - 12.50 m		40	20	92	95	97	99	99	100	100	100	100	100	100	100	100	100	100	100	100	100	100	249
-	N504 B-1; 13.72 m - 14.02 m		37	23		93	96	97	98	98	99	99	100	100	100	100	100	100	100	100	100	100	100	250
-	N504 B-1; 15.24 m - 15.48 m		42	25	72	77	80	82	84	88	91	93	97	98	99	100	100	100	100	100	100	100	100	251
-	N504 B-2; 4.57 m - 5.03 m	SM	NV	NP	25	52	84	95	98	99	100	100	100	100	100	100	100	100	100	100	100	100	100	260
_	N504 B-3; 3.05 m - 3.51 m	SC	35	22	45	52	70	78	81	82	82	83	84	84	84	84	86	86	100	100	100	100	100	272
	N504 B-4; 1.52 m - 1.98 m	CL	37	23	58	68	88	95	98	99	99	99	100	100	100	100	100	100	100	100	100	100	100	285
T	N504 B-4; 7.62 m - 8.08 m	SP-SM	NV	NP	7.6	18	39	47	51	53	54	55	60	63	69	73	86	90	100	100	100	100	100	288
	N504 B-1; 0.00 m - 1.52 m	SM	NV	NP	27	48	75	86	90	92	93	93	95	95	97	98	99	99	99	100	100	100	100	300
Г	N504 B-3; 0.00 m - 1.52 m	SC	30	16	37	51	75	85	90	93	94	95	97	98	99	99	100	100	100	100	100	100	100	302



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**PROJECT:** BIA project N12(12-2)(19-2)2+4

LOCATION: Navajo, NM to N64 junction AZ (near Tsaile, AZ)

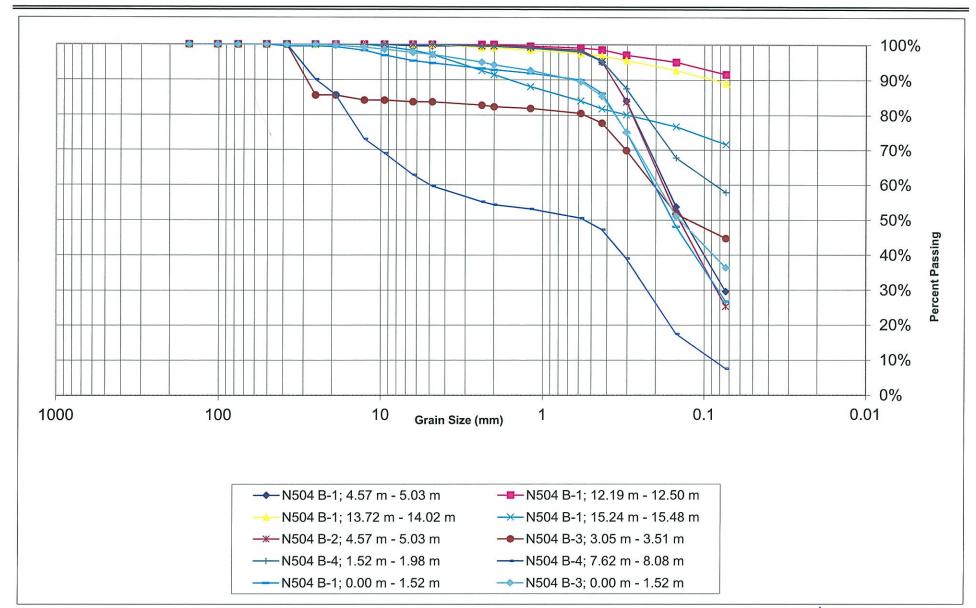
SAMPLE SOURCE: SEE BELOW

**JOB NO:** 1720134030.0002

WORK ORDER NO: 3

DATE ASSIGNED: 10/2/13

#### **MECHANICAL SIEVE ANALYSIS**





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

1720134030.0002

WORK ORDER NO: DATE ASSIGNED:

11/4/13

Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00) Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05) GROUP SYMBOL, USCS (ASTM D-2487)

#### SIEVE SIZES

Silt or		SAND			GRAVEL	COBBLES
Clay	Fine	Medium	Coarse	Fine	Coarse	GODDELO
Location & Depth USCS LL PI 75um	150um 300um 425um	600um   1.18um   2.00mm	2.36mm 4.75mm	6.3mm   9.5mm   12.5mm   19mm	25mm 31.2mm 37.5mm 50mm 75mm	152mm Lab#

#### PERCENT PASSING BY WEIGHT

N503 B-1 @ 0.00 m - 1.52 m	SC-SM	21	7	30	40	54	60	63	68	72	74	82	85	90	94	97	98	99	100	100	100	100	372
N503 B-3 @ 0.00 m - 1.52 m	CL-ML	22	6	50	65	80	86	89	91	93	94	96	97	98	99	100	100	100	100	100	100	100	374
N613 B-2 @ 0.00 m - 1.52 m	SC	28	14	48	62	70	73	75	78	81	82	87	90	94	96	98	99	100	100	100	100	100	377
N614 B-3 @ 0.00 m 1.52 m	SC	27	13	32	37	42	44	47	52	57	60	69	73	80	85	90	94	96	97	100	100	100	382
N505 B-4 @ 0.00 m - 1.52 m	CL	29	14	54	70	80	84	86	88	89	89	91	93	96	98	100	100	100	100	100	100	100	386
N503 B-1 @ 2.44 m -2.90 m	CL	30	11	51	58	64	66	68	71	74	75	81	83	84	85	85	85	100	100	100	100	100	387
N503 B-1 @ 5.49 m - 5.94 m	ML	NV	NP	67	89	95	96	97	98	99	99	100	100	100	100	100	100	100	100	100	100	100	389
N503 B-1 @ 7.01 m - 7.47 m	GM	NV	NP	18	26	33	38	43	47	49	50	56	59	65	71	90	95	100	100	100	100	100	390
N503 B-2 @ 1.52 m - 1.98 m	CL-ML	26	7	63	71	78	82	84	88	90	92	96	98	100	100	100	100	100	100	100	100	100	391
N503 B-2 @ 3.05 m - 3.51 m	CL	30	8	52	59	67	71	74	79	83	85	90	92	94	95	100	100	100	100	100	100	100	392



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**PROJECT:** BIA project N12(12-2)(19-2)2+4

LOCATION: Navajo, NM to N64 junction AZ (near Tsaile, AZ)

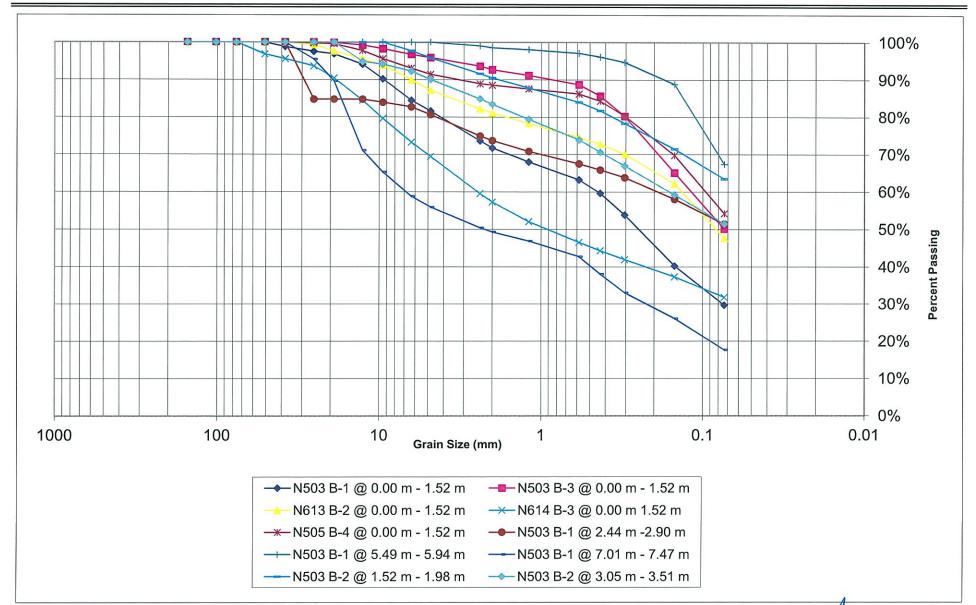
SAMPLE SOURCE: SEE BELOW

**JOB NO:** 1720134030.0002

WORK ORDER NO: 4

DATE ASSIGNED: 11/4/13

#### **MECHANICAL SIEVE ANALYSIS**





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

1720134030.0002

WORK ORDER NO:

4 11/4/13

DATE ASSIGNED:

Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00)
Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05)
GROUP SYMBOL, USCS (ASTM D-2487)

#### SIEVE SIZES

Si	ilt or			SAND								GRAVE	L				COBBLES	
C	lay	Fine	Fine Medium				arse		Fir	ne				Coarse			GODDELO	
Location & Depth USCS LL PI 7	5um 1	150um 300um 425ur	1 600um	1.18um	2.00mm	2.36mm	4.75mm	6.3mm	9.5mm	12.5mm	19mm	25mm	31.2mm	37.5mm	50mm	75mm	152mm	Lab#

#### PERCENT PASSING BY WEIGHT

																			and the second second second	110000000000000000000000000000000000000		Section of the second section of the section of the second section of the section of the second section of the sectio	
N503 B-2 @ 6.10 m - 6.40 m	GM	NV	NP	13	18	25	30	34	39	42	43	50	53	61	64	78	93	100	100	100	100	100	393
N503 B-3 @ 3.05 m - 3.51 m	ML	19	3	51	68	84	89	92	95	96	96	98	98	99	100	100	100	100	100	100	100	100	397
N503 B-3 @ 6.10 m -6.55 m	GP-GM	NV	NP	11	17	25	30	34	37	39	41	47	51	61	67	82	89	100	100	100	100	100	398
N503 B-3 @ 7.62 m - 8.08 m	SP-SM	NV	NP	9.1	15	25	32	37	42	45	47	55	59	69	77	90	100	100	100	100	100	100	399
N503 B-3 @ 9.14 m - 9.45 m	SM	NV	NP	12	16	23	27	32	38	41	44	57	62	72	80	84	100	100	100	100	100	100	400
N503 B-3 @ 10.67 m - 10.97 m	SC-SM	23	6	22	25	31	34	38	44	51	55	69	76	88	91	100	100	100	100	100	100	100	401
N503 B-4 @ 1.52 m - 1.98 m	SM	NV	NP	41	57	74	80	83	86	88	88	89	90	93	96	100	100	100	100	100	100	100	402
N503 B-4 @ 4.57 m - 5.03 m	GM	NV	NP	16	21	28	32	34	38	40	42	47	49	57	61	74	100	100	100	100	100	100	403
N503 B-4 @ 6.10 m - 6.55 m	SM	NV	NP	40	62	83	91	95	97	98	98	99	100	100	100	100	100	100	100	100	100	100	404
N503 B-4 @ 7 62 m - 8 08 m	SP	NV	NP	1.6	7	27	44	52	57	58	59	63	66	71	77	87	100	100	100	100	100	100	405



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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

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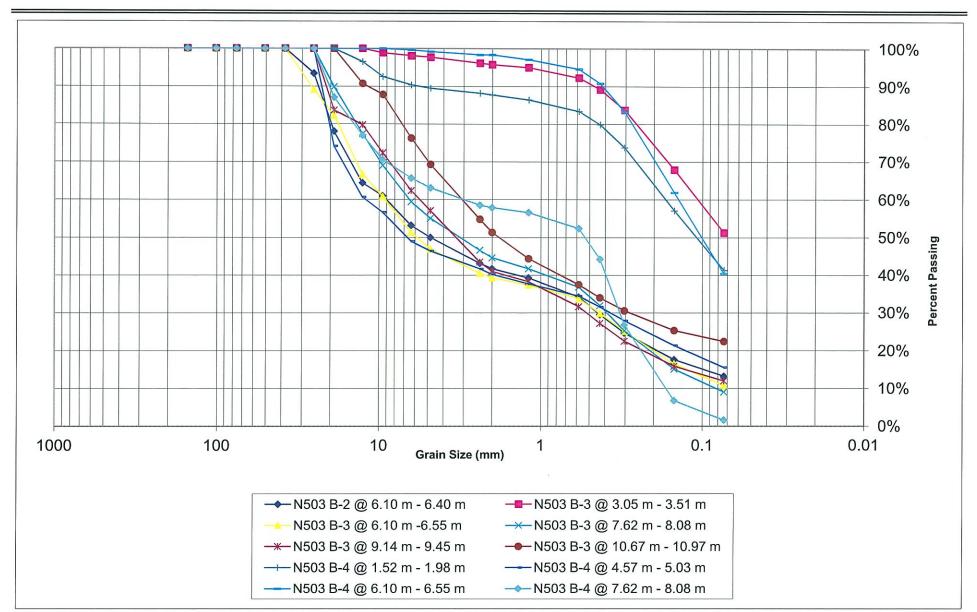
JOB NO:

1720134030.0002

WORK ORDER NO: DATE ASSIGNED:

11/4/13

#### **MECHANICAL SIEVE ANALYSIS**









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

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JOB NO:

1720134030.0002

WORK ORDER NO:

4

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Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00)
Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05)
GROUP SYMBOL, USCS (ASTM D-2487)

#### SIEVE SIZES

Silt or		SAND ,			GRAVEL	COBBLES
Clay	Fine	Medium	Coarse	Fine	Coarse	
Location & Depth USCS LL PI 75um	150um 300um 425um	600um 1.18um 2.00mm	2.36mm 4.75mm	6.3mm   9.5mm   12.5mm   19mm	25mm 31.2mm 37.5mm 50mm 75mm	152mm Lat

#### PERCENT PASSING BY WEIGHT

N613 B-1 @ 1.52 m - 1.98 m	SM	NV	NP	30	58	81	86	90	94	95	96	97	98	99	100	100	100	100	100	100	100	100	406
N613 B-1 @ 4.57 m - 5.03 m	-	NV	NP	30	57	79	86	90	94	96	96	98	99	99	100	100	100	100	100	100	100	100	407
N613 B-1 @ 6.10 m - 6.25 m	SM	NV	NP	20	50	84	91	94	97	98	98	99	99	99	100	100	100	100	100	100	100	100	408
N613 B-2 @ 3.05 m - 3.51 m	SM	NV	NP	31	78	97	99	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	410
N613 B-2 @ 6.10 m - 6.55 m		NV	NP	37	72	85	92	96	99	100	100	100	100	100	100	100	100	100	100	100	100	100	411
	SP-SM	-	-	8.8	24	58	72	79	83	85	85	86	87	88	88	88	88	100	100	100	100	100	412
N613 B-3 @ 1.52 m - 1.98 m		-	NP	27	66	93	97	98	100	100	100	100	100	100	100	100	100	100	100	100	100	100	413
N613 B-3 @ 4.57 m - 5.03 m		NV	-	17	54	85	93	97	99	100	100	100	100	100	100	100	100	100	100	100	100	100	414
N613 B-3 @ 6.10 m - 6.55 m	SC	27	9	37	73	93	95	96	97	98	98	99	100	100	100	100	100	100	100	100	100	100	415
N613 B-3 @ 9 14 m - 9 60 m	CI	44	27	75	92	98	99	99	100	100	100	100	100	100	100	100	100	100	100	100	100	100	416



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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

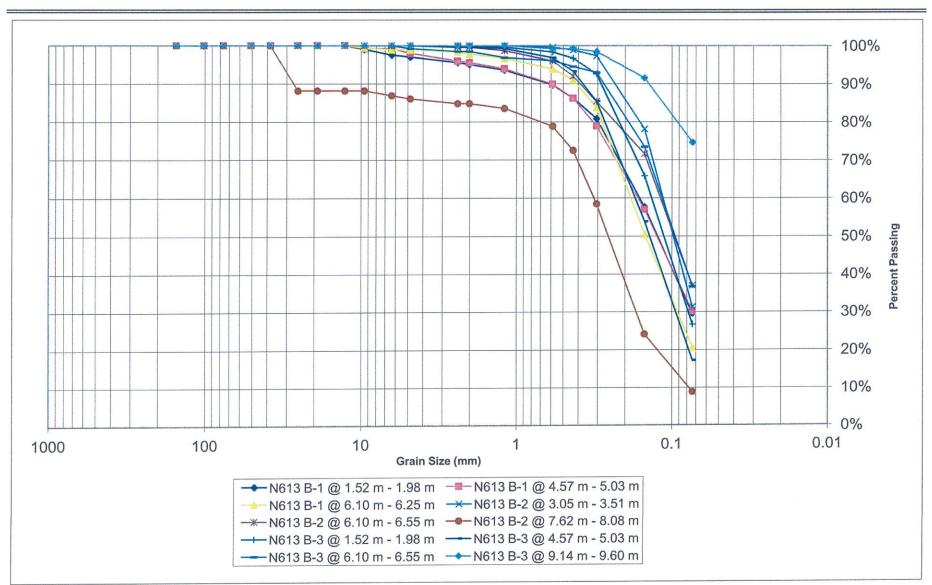
JOB NO:

1720134030.0002

WORK ORDER NO: DATE ASSIGNED:

11/4/13

#### **MECHANICAL SIEVE ANALYSIS**







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

1720134030.0002

WORK ORDER NO:

DATE ASSIGNED:

11/4/13

Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00)
Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05)
GROUP SYMBOL, USCS (ASTM D-2487)

#### SIEVE SIZES

Silt or		SAND			GRAVEL	COBBLES	
Clay	Fine	Medium	Coarse	Fine	Coarse		
Location & Depth USCS LL PI 75um	150um 300um 425un	600um 1.18um 2.00mm	2.36mm 4.75mm	6.3mm   9.5mm   12.5mm   19mm	25mm 31.2mm 37.5mm 50mm 75mm	152mm La	ab#

#### PERCENT PASSING BY WEIGHT

N613 B-3 @ 10.67 m - 11.13 m	CI	37	23	77	90	95	97	98	98	99	99	100	100	100	100	100	100	100	100	100	100	100	417
N613 B-3 @ 13.72 m - 14.17 m	SM	-	NP	33	48	61	68	73	83	89	91	95	96	96	99	100	100	100	100	100	100	100	418
N613 B-3 @ 15.24 m - 15.70 m	SM	-	NP	34	44	48	53	58	70	78	81	90	94	97	100	100	100	100	100	100	100	100	419
N613 B-4 @ 1.52 m - 1.98 m	SM	-	NP	36	74	94	97	98	99	100	100	100	100	100	100	100	100	100	100	100	100	100	420
N613 B-4 @ 7.62 m - 8.08 m	SP-SM	NV	NP	5.3	19	53	74	84	92	95	96	99	100	100	100	100	100	100	100	100	100	100	421
N613 B-4 @ 9.14 m - 9.60 m	CL	-	-		80	90	94	96	98	99	99	100	100	100	100	100	100	100	100	100	100	100	422
N613 B-4 @ 10.67 m - 11.13 m	ML	NV	NP	71	80	88	90	91	93	94	95	98	99	100	100	100	100	100	100	100	100	100	423
N614 B-1 @ 3.05 m - 3.51 m	SM	NV	NP	39	70	95	99	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	424
N614 B-1 @ 4.57 m - 5.03 m	CL-ML	24	7	50	79	95	98	99	100	100	100	100	100	100	100	100	100	100	100	100	100	100	425
N614 B-1 @ 7 62 m - 8 08 m	SP-SM	NV	NP	5.6	18	49	67	86	99	100	100	100	100	100	100	100	100	100	100	100	100	100	426



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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

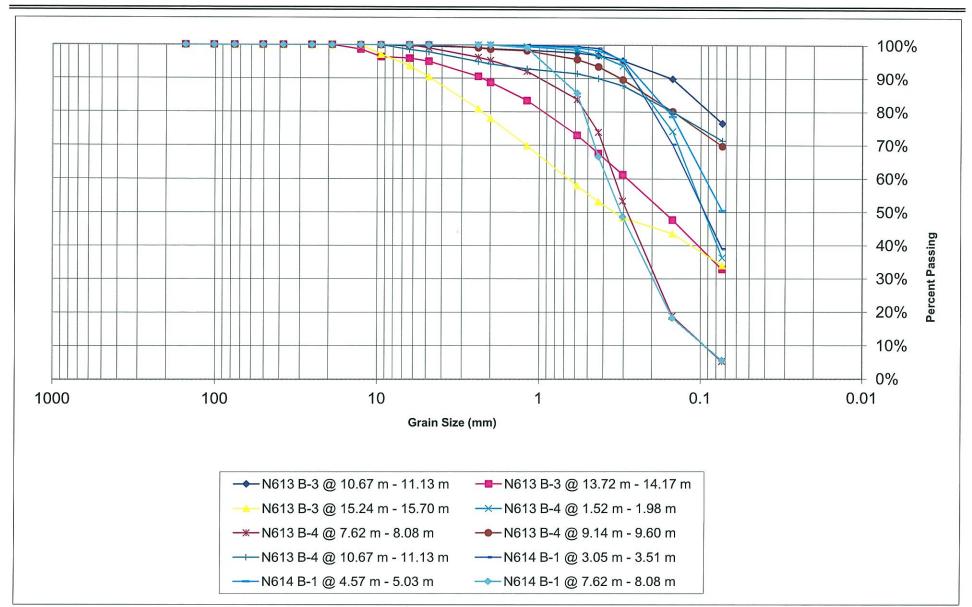
1720134030.0002

WORK ORDER NO:

4

DATE ASSIGNED: 11/4/13

#### **MECHANICAL SIEVE ANALYSIS**









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

1720134030.0002

WORK ORDER NO:

DATE ASSIGNED:

11/4/13

Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00)
Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05)
GROUP SYMBOL, USCS (ASTM D-2487)

### SIEVE SIZES

	Silt or		SAND				GRAVEL						COBBLES					
	Clay	Fine		Medium		Coa	rse		Fi	ne				Coarse				
Location & Depth USCS LL	PI 75um	150um 300um 425u	n 600um 1	1.18um	2.00mm	2.36mm	4.75mm	6.3mm	9.5mm	12.5mm	19mm	25mm	31.2mm	37.5mm	50mm	75mm	152mm	Lab#

### PERCENT PASSING BY WEIGHT

N614 B-1 @ 9.14 m - 9.60 m	SM	NV	NP	13	17	31	45	58	71	76	77	81	83	87	92	94	100	100	100	100	100	100	427
N614 B-1 @ 10.67 m - 11.13 m	SP-SM	NV	NP	5.6	12	60	82	91	95	97	97	98	98	100	100	100	100	100	100	100	100	100	428
N614 B-2 @ 3.05 m - 3.51 m	SC	28	12	38	45	54	58	63	70	73	74	80	83	88	93	100	100	100	100	100	100	100	430
N614 B-2 @ 6.1 m - 6.55 m	SM	NV	NP	34	68	97	99	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	431
N614 B-2 @ 9.14 m - 9.60 m	SP-SM	ŃV	NP	6.3	15	46	70	86	94	96	97	98	99	99	100	100	100	100	100	100	100	100	432
N614 B-3 @ 1.52 m - 1.98 m	GC	30	15	33	39	44	46	48	54	56	58	65	68	76	79	85	85	100	100	100	100	100	433
N614 B-3 @ 3.05 m - 3.51 m	CL	32	16	53	65	77	81	83	87	90	91	95	97	99	100	100	100	100	100	100	100	100	434
N614 B-3 @ 6.10 m - 6.55 m	SM	NV	NP	41	57	69	73	76	83	87	89	96	97	99	100	100	100	100	100	100	100	100	435
N614 B-4 @ 1.52 m - 1.98 m	SC	29	13		42	47	50	52	59	64	66	74	77	84	90	100	100	100	100	100	100	100	436
N614 B-4 @ 4.57 m - 5.03 m	SC	-	24		29	39	46	54	70	74	74	79	80	84	85	100	100	100	100	100	100	100	437



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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

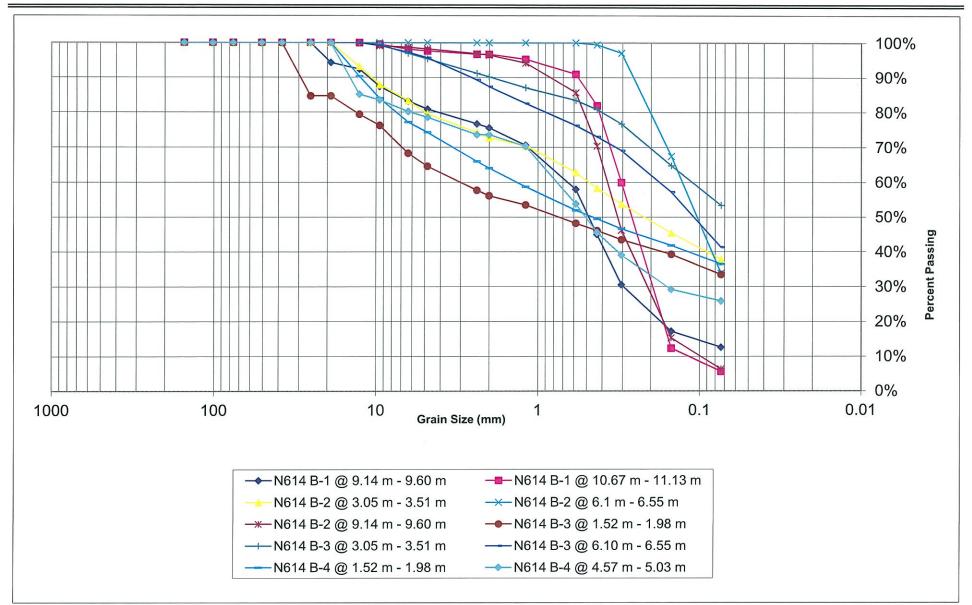
1720134030.0002

WORK ORDER NO:

DATE ASSIGNED:

11/4/13

### **MECHANICAL SIEVE ANALYSIS**









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

SAMPLE SOURCE:

SEE BELOW

JOB NO:

1720134030.0002

WORK ORDER NO:

.

DATE ASSIGNED:

11/4/13

Liquid Limit, Plastic Limit & Plasticity Index (AASHTO T89-10 & T90-00)
Sieve Analysis of Fine and Coarse Aggregates (AASHTO T27-11 & T11-05)
GROUP SYMBOL, USCS (ASTM D-2487)

### SIEVE SIZES

Silt or		SAND			COBBLES	
Clay	Fine	Medium	Coarse	Fine	Coarse	10000000
Location & Depth USCS LL PI 75um	150um 300um 425um	600um 1.18um 2.00mm	2.36mm 4.75mm	6.3mm 9.5mm 12.5mm 19m	m 25mm 31.2mm 37.5mm 50mm 75mm	152mm Lab

### PERCENT PASSING BY WEIGHT

N614 B-4 @ 6.10 m - 6.55 m	SC	28	11	43	50	54	57	59	65	70	72	80	82	85	86	86	86	100	100	100	100	100	438
N614 B-4 @ 7.62 m - 8.08 m			7	38	42	47	50	54	65	73	76	86	89	94	95	100	100	100	100	100	100	100	439
N614 B-4 @ 9.14 m - 9.45 m	-	NV	NP	23	26	30	33	36	44	52	55	66	73	77	80	90	100	100	100	100	100	100	44
N505 B-1 3.05 m - 3.20 m	GC	25	12	-	33	45	48	49	50	51	51	53	55	58	61	65	78	100	100	100	100	100	44
N505 B-2 @ 1.52 m - 1.98 m	sc	26	13	39	60	69	72	74	80	84	86	92	94	97	97	100	100	100	100	100	100	100	44
N505 B-2 @ 3.81 m - 3.96 m	SC	34	14	43	56	69	75	80	92	97	99	100	100	100	100	100	100	100	100	100	100	100	44
N505 B-3 @ 1.22 m - 1.68 m	CL	36	20	75	89	95	97	97	98	98	99	99	99	100	100	100	100	100	100	100	100	100	44
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REVIEWED BY

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**PROJECT:** BIA project N12(12-2)(19-2)2+4

LOCATION: Navajo, NM to N64 junction AZ (near Tsaile, AZ)

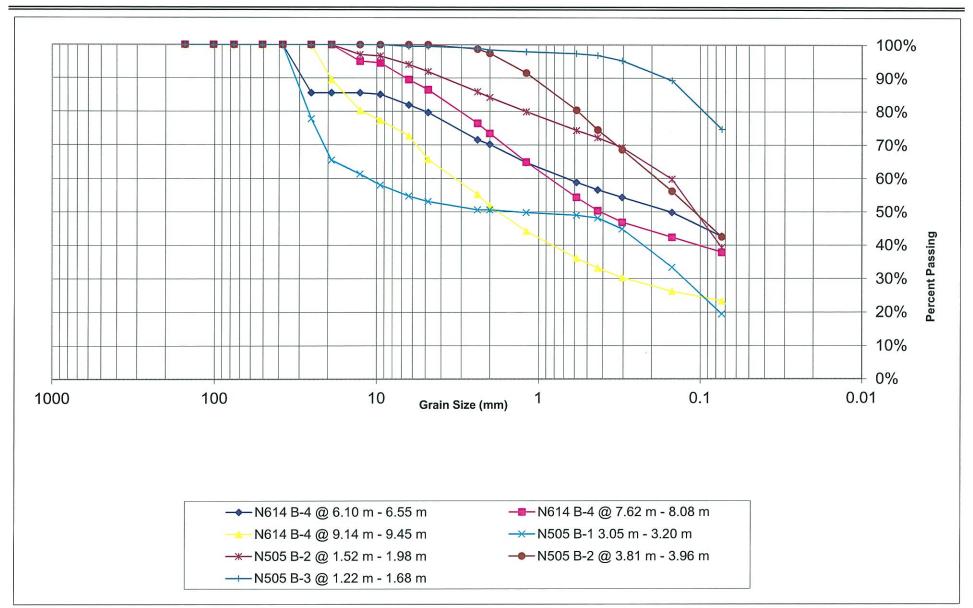
SAMPLE SOURCE: SEE BELOW

**JOB NO:** 1720134030.0002

WORK ORDER NO:

DATE ASSIGNED: 11/4/13

### **MECHANICAL SIEVE ANALYSIS**







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

SAMPLE PREPARATION:

N503 B-1 @ 3.81 m - 4.27 m

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

4

LAB NO:

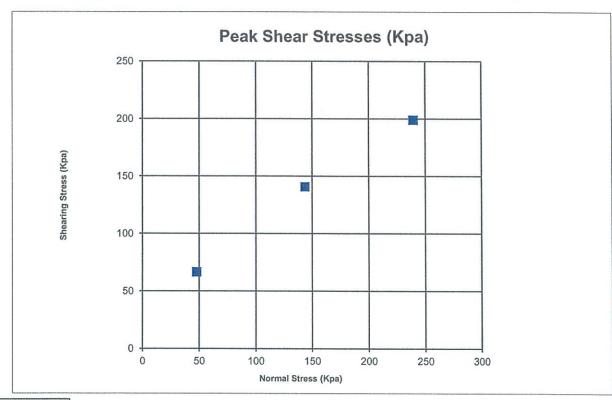
445

DATE ASSIGNED:

11/4/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automated Shear	Test System by Trautwein S	Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	47.9	143.6	239.4
Dry mass of specimen (g):	124.0	124.7	122.9
Initial Moisture Content:	19.5%	16.9%	21.7%
Initial Wet Density (Kg per cu.m):	1965.4	1934.2	1984.1
Initial Dry Density (Kg per cu.m):	1645.0	1654.6	1631.0
Final Moisture Content:	31.0%	27.5%	30.6%
Final Wet Density (Kg per cu.m):	2153.3	2108.9	2128.8
Final Dry Density (Kg per cu.m):	1644.2	1653.9	1630.3
Normal Stress (kpa):	47.9	143.6	239.4
Maximum Shearing Stress (Kpa):	66.51	140.65	198.89
Vertical Deformation @ Max Shear (mm):	0.245	-0.004	-0.190
Horizontal Deformation @ Max Shear (mm):	2.892	3.422	12.628







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N503 B-1 @ 3.81 m - 4.27 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

LAB NO:

445

DATE ASSIGNED:

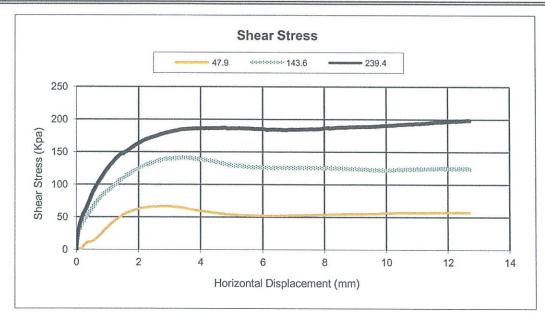
11/4/2013

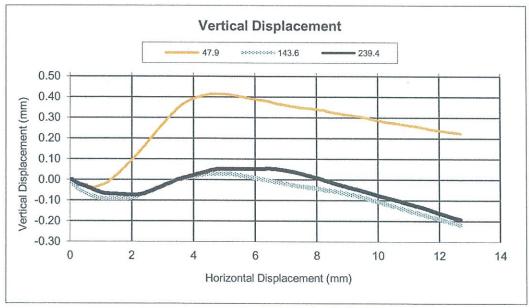
NORMAL LOADS (Kpa):

47.9

143.6

239.4







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

Insitu-Saturate

SAMPLE PREPARATION:

SAMPLE SOURCE:

N503 B-2 @ 7.62 m - 7.92 m

JOB NO:

1720134030.0002

WORK ORDER NO:

LAB NO:

447

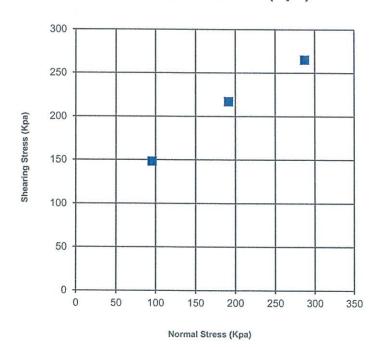
DATE ASSIGNED:

11/4/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4			
Initial diameter of specimen (mm):	61.5			
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipme	nt
Rate of deformation (mm/min):	0.4064		5 1 40	
Direct shear point (Kpa):	95.8	191.5	287.3	
Dry mass of specimen (g):	137.7	140.1	139.6	
Initial Moisture Content:	18.1%	18.0%	17.4%	
Initial Wet Density (Kg per cu.m):	2155.5	2191.1	2174.0	
Initial Dry Density (Kg per cu.m):	1826.2	1858.0	1852.1	
Final Moisture Content:	19.3%	20.1%	18.7%	
Final Wet Density (Kg per cu.m):	2177.7	2229.9	2198.2	
Final Dry Density (Kg per cu.m):	1825.4	1857.2	1851.2	
Normal Stress (kpa):	95.8	191.5	287.3	
Maximum Shearing Stress (Kpa):	148.38	217.14	265.42	
Vertical Deformation @ Max Shear (mm):	0.124	-0.416	0.004	
Horizontal Deformation @ Max Shear (mm):	12.626	12.696	11.437	

# Peak Shear Stresses (Kpa)







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N503 B-2 @ 7.62 m - 7.92 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

4

LAB NO:

447

DATE ASSIGNED:

11/4/2013

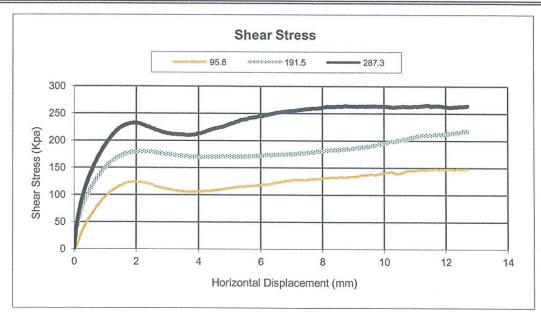
NORMAL LOADS (Kpa):

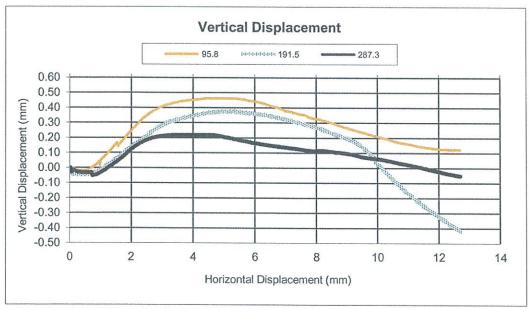
95.8

191.5

287.3

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: SAMPLE PREPARATION: N503 B-4 @ 9.14 m - 9.45 m

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

LAB NO:

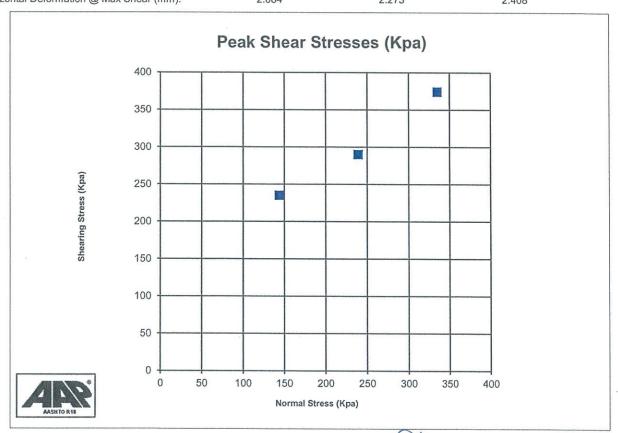
451

DATE ASSIGNED:

11/4/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25,4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	utwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	143.6	239.4	335.2
Dry mass of specimen (g):	153.2	154.7	152.4
Initial Moisture Content:	13.3%	12.0%	12.4%
Initial Wet Density (Kg per cu.m):	2300.5	2296.4	2270.3
Initial Dry Density (Kg per cu.m):	2032.2	2052.1	2021.5
Final Moisture Content:	15.6%	14.4%	14.8%
Final Wet Density (Kg per cu.m):	2349.2	2347.0	2320.5
Final Dry Density (Kg per cu.m):	2031.3	2051.2	2020.6
Normal Stress (kpa):	143.6	239.4	335.2
Maximum Shearing Stress (Kpa):	235.00	289.99	374.09
Vertical Deformation @ Max Shear (mm):	0.307	0.205	0.168
Horizontal Deformation @ Max Shear (mm):	2.084	2.273	2.408





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N503 B-4 @ 9.14 m - 9.45 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

LAB NO:

451

DATE ASSIGNED:

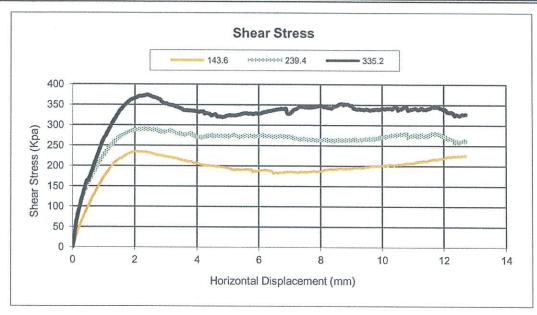
11/4/2013

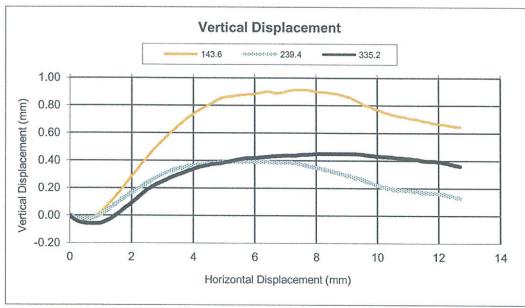
NORMAL LOADS (Kpa):

143.6

239.4

335.2







PROJECT: LOCATION:

MATERIAL:

BIA project N12(12-2)(19-2)2+4

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

Bore hole samples

SAMPLE SOURCE:

N504 B-1; 16.76 m -17.07 m

SAMPLE PREPARATION:

Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

LAB NO:

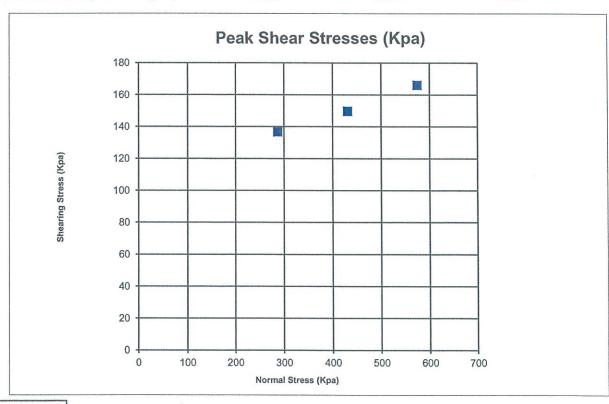
3 313

DATE ASSIGNED:

10/2/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Train	utwein Soil Testing Equipmer
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	287.3	430.9	574.6
Dry mass of specimen (g):	136.7	136.8	139.8
Initial Moisture Content:	18.3%	18.6%	16.7%
Initial Wet Density (Kg per cu.m):	2143.2	2153.0	2164.0
Initial Dry Density (Kg per cu.m):	1812.9	1815.4	1854.8
Final Moisture Content:	21.8%	19.1%	17.4%
Final Wet Density (Kg per cu.m):	2206.9	2161.0	2176.4
Final Dry Density (Kg per cu.m):	1812.1	1814.6	1854.0
Normal Stress (kpa):	287.3	430.9	574.6
Maximum Shearing Stress (Kpa):	136.64	149.59	165.95
Vertical Deformation @ Max Shear (mm):	-0.192	-0.300	-0.386
Horizontal Deformation @ Max Shear (mm):	6.686	12.355	12.514





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

SAMPLE SOURCE:

Bore hole samples

N504 B-1; 16.76 m -17.07 m

SAMPLE PREPARATION: Saturate

LAB NO:

JOB NO:

1720134030.0002

WORK ORDER NO: 3

313

DATE ASSIGNED:

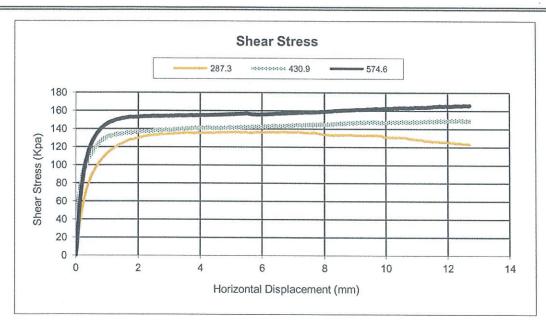
10/2/2013

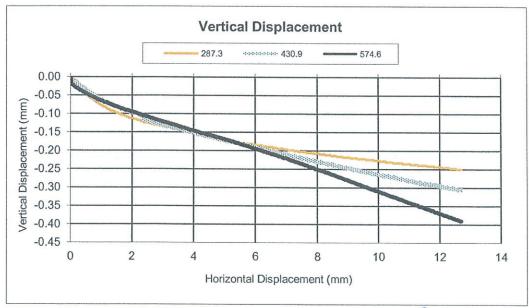
NORMAL LOADS (Kpa):

287.3

430.9

574.6







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N504 B-2; 3.20 m - 3.35 m

SAMPLE PREPARATION: Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

LAB NO:

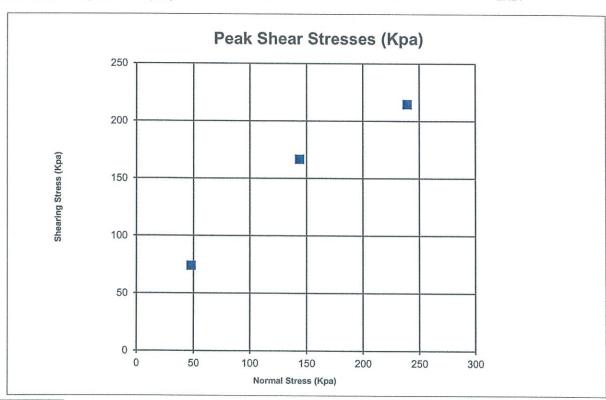
316

DATE ASSIGNED:

10/2/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automated	d Shear Test System by Tra	utwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	47.9	143.6	239.4
Dry mass of specimen (g):	139.8	143.2	141.1
Initial Moisture Content:	13.2%	12.3%	13.6%
Initial Wet Density (Kg per cu.m):	2097.7	2131.3	2126.1
Initial Dry Density (Kg per cu.m):	1854.2	1899.3	1872.1
Final Moisture Content:	16.5%	16.9%	18.9%
Final Wet Density (kg per cu.m):	2159.7	2219.5	2224.5
Final Dry Density (kg per cu.m)):	1853.3	1898.4	1871.2
Normal Stress (kpa):	47.9	143.6	239.4
Maximum Shearing Stress (Kpa):	73.97	166.58	214.57
Vertical Deformation @ Max Shear (mm):	0.348	0.198	0.209
Horizontal Deformation @ Max Shear (mm):	1.928	1.679	2.424





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N504 B-2; 3.20 m - 3.35 m

SAMPLE PREPARATION: Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 3

J. 3

LAB NO:

316

DATE ASSIGNED:

10/2/2013

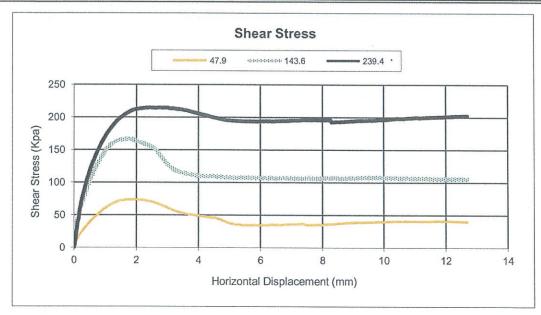
NORMAL LOADS (Kpa):

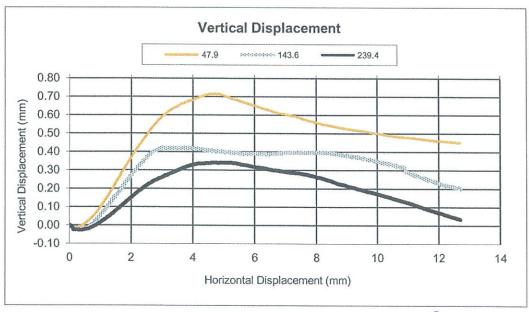
47.9

143.6

239.4

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)





Duy



BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: SAMPLE PREPARATION: N504 B-3; 7.01 m - 7.32 m

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

3

LAB NO:

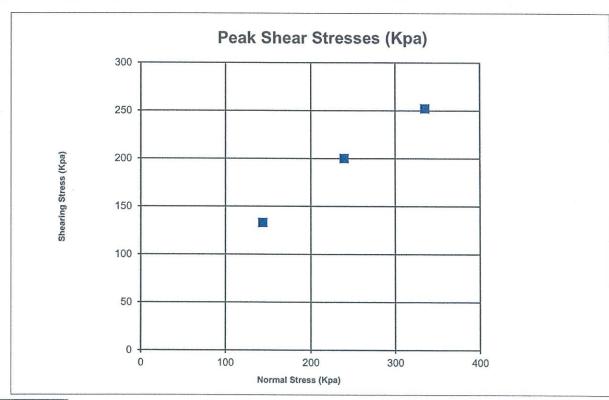
323

DATE ASSIGNED:

10/2/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	143.6	239.4	335.2
Dry mass of specimen (g):	124.6	125.7	125.5
Initial Moisture Content:	23.0%	21.0%	22.4%
Initial Wet Density (Kg per cu.m):	2032.2	2016.6	2037.4
Initial Dry Density (Kg per cu.m):	1653.3	1667.1	1664.7
Final Moisture Content:	22.9%	22.8%	22.5%
Final Wet Density (kg per cu.m):	2030.9	2046.3	2038.5
Final Dry Density (kg per cu.m):	1652.6	1666.4	1664.0
Normal Stress (kpa):	143.6	239.4	335.2
Maximum Shearing Stress (Kpa):	132.91	200.01	252.17
Vertical Deformation @ Max Shear (mm):	0.169	0.113	0.039
Horizontal Deformation @ Max Shear (mm):	2.830	2.186	1.939







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N504 B-3; 7.01 m - 7.32 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 3

LAB NO:

323

DATE ASSIGNED:

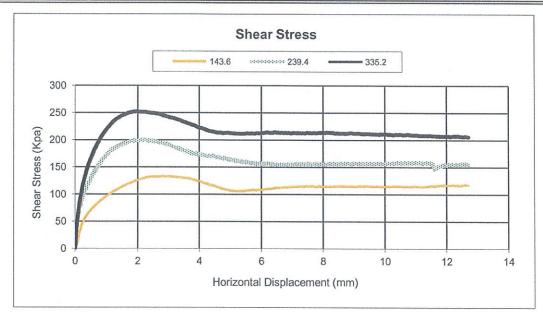
10/2/2013

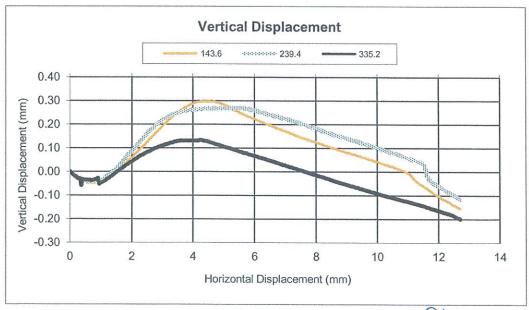
NORMAL LOADS (Kpa):

143.6

239.4

335.2







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N505 B-1 @ 1.52 m - 1.83 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

4

LAB NO:

465

DATE ASSIGNED:

11/4/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		- 1 -
Direct shear point (Kpa):	47.9	143.6	239.4
Dry mass of specimen (g):	134.1	133.0	137.7
Initial Moisture Content:	10.4%	11.2%	9.9%
Initial Wet Density (Kg per cu.m):	1963.7	1961.9	2006.1
Initial Dry Density (Kg per cu.m):	1779.5	1764.8	1826.6
Final Moisture Content:	23.6%	20.6%	22.1%
Final Wet Density (Kg per cu.m):	2199.3	2128.1	2228.4
Final Dry Density (Kg per cu.m):	1778.7	1764.0	1825.8
Normal Stress (kpa):	47.9	143.6	239.4
Maximum Shearing Stress (Kpa):	45.62	116.38	185.05
Vertical Deformation @ Max Shear (mm):	-0.183	-0.505	-0.362
Horizontal Deformation @ Max Shear (mm):	12.370	12.704	10.818

# Peak Shear Stresses (Kpa) 200 150 100 50 Normal Stress (Kpa)



BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N505 B-1 @ 1.52 m - 1.83 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

LAB NO:

465

DATE ASSIGNED:

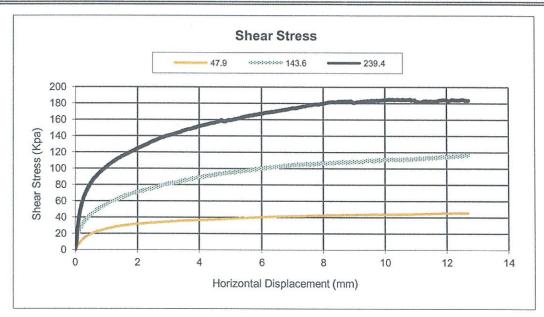
11/4/2013

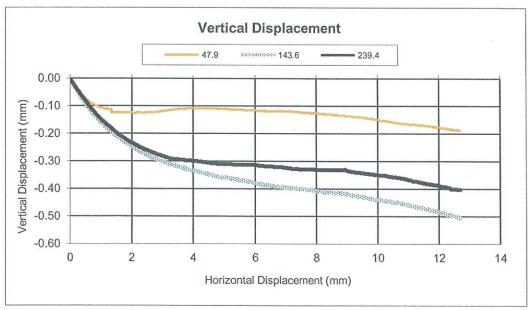
NORMAL LOADS (Kpa):

47.9

143.6

239.4









BIA project N12(12-2)(19-2)2+4

N505 B-2 @ 2.29 m - 2.59 m

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE PREPARATION:

SAMPLE SOURCE:

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

LAB NO:

466

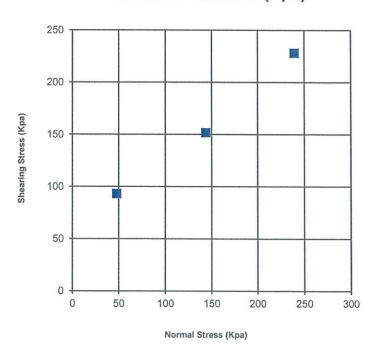
DATE ASSIGNED:

11/4/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064	50 10 Second Military 2010 (2010 E. 2000)	30 annian air 190 annia 190 annia 197
Direct shear point (Kpa):	47.9	143.6	239.4
Dry mass of specimen (g):	143.0	144.3	148.7
Initial Moisture Content:	10.5%	12.3%	12.1%
Initial Wet Density (Kg per cu.m):	2094.7	2148.8	2209.7
Initial Dry Density (Kg per cu.m):	1896.5	1914.4	1972.4
Final Moisture Content:	21.0%	18.0%	17.3%
Final Wet Density (Kg per cu.m):	2294.4	2258.1	2311.9
Final Dry Density (Kg per cu.m):	1895.6	1913.5	1971.5
Normal Stress (kpa):	47.9	143.6	239.4
Maximum Shearing Stress (Kpa):	93.05	151.71	228.04
Vertical Deformation @ Max Shear (mm):	0.896	-0.051	0.205
Horizontal Deformation @ Max Shear (mm):	12.704	12.672	8.752

# Peak Shear Stresses (Kpa)





REVIEWED BY LUU



BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N505 B-2 @ 2.29 m - 2.59 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

LAB NO:

466

DATE ASSIGNED:

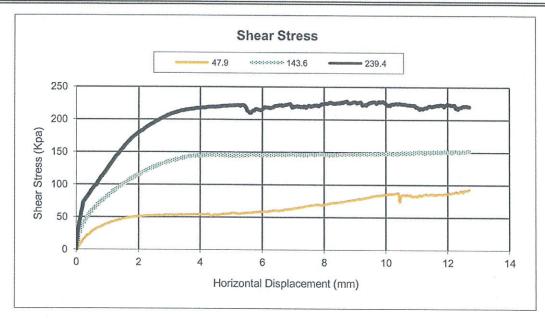
11/4/2013

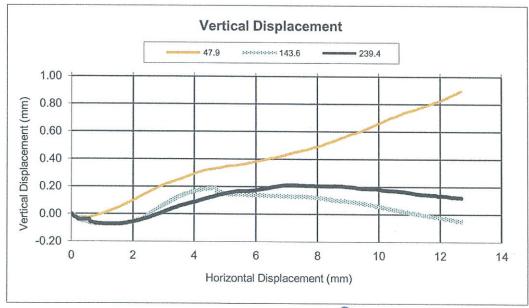
NORMAL LOADS (Kpa):

47.9

143.6

239.4







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N505 B-4 @ 1.52 m - 1.83 m

SAMPLE PREPARATION:

Insitu-Saturate

JOB NO:

1720134030 0002

WORK ORDER NO:

4

LAB NO:

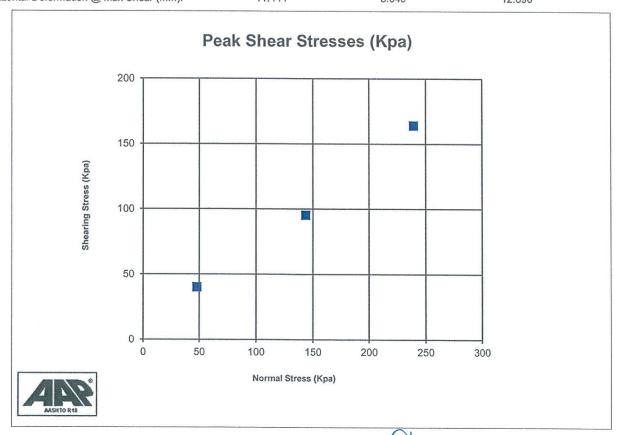
467

DATE ASSIGNED:

11/4/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064	2 12.	
Direct shear point (Kpa):	47.9	143.6	239.4
Dry mass of specimen (g):	122.5	121.4	126.1
Initial Moisture Content:	10.8%	11.7%	12.1%
Initial Wet Density (Kg per cu.m):	1799.1	1797.6	1873.1
Initial Dry Density (Kg per cu.m):	1624.5	1610.2	1672.3
Final Moisture Content:	29.9%	30.5%	27.6%
Final Wet Density (Kg per cu.m):	2109.1	2100.7	2133.4
Final Dry Density (Kg per cu.m):	1623.8	1609.5	1671.5
Normal Stress (kpa):	47.9	143.6	239.4
Maximum Shearing Stress (Kpa):	40.09	95.25	163.99
Vertical Deformation @ Max Shear (mm):	-0.506	-0.680	-0.713
Horizontal Deformation @ Max Shear (mm):	11.444	8.649	12.696





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N505 B-4 @ 1.52 m - 1.83 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

LAB NO:

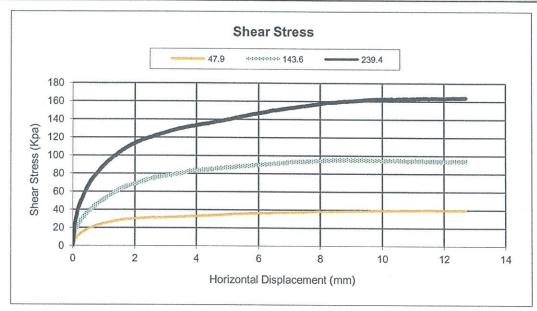
DATE ASSIGNED: 11/4/2013

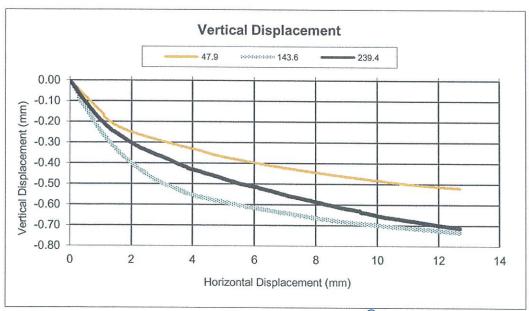
NORMAL LOADS (Kpa):

47.9

143.6

239.4







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE PREPARATION:

SAMPLE SOURCE:

N613 B-1 @ 3.05 m - 3.35 m Insitu-Saturate JOB NO:

1720134030.0002

WORK ORDER NO:

4

LAB NO:

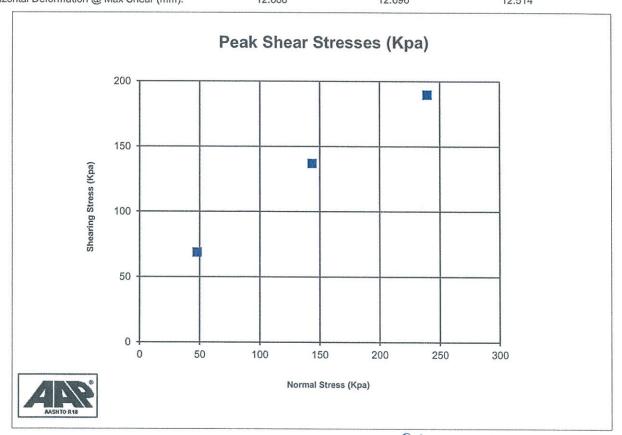
452

DATE ASSIGNED:

11/4/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automated	Shear Test System by Tra	utwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	47.9	143.6	239.4
Dry mass of specimen (g):	125.8	127.7	133.4
Initial Moisture Content:	10.8%	10.6%	11.8%
Initial Wet Density (Kg per cu.m):	1849.0	1873.4	1978.3
Initial Dry Density (Kg per cu.m):	1669.2	1694.2	1769.8
Final Moisture Content:	26.7%	25.7%	24.6%
Final Wet Density (Kg per cu.m):	2114.7	2128.6	2204.0
Final Dry Density (Kg per cu.m):	1668.5	1693.4	1769.0
Normal Stress (kpa):	47.9	143.6	239.4
Maximum Shearing Stress (Kpa):	68.77	136.92	189.61
Vertical Deformation @ Max Shear (mm):	0.228	-0.438	-0.543
Horizontal Deformation @ Max Shear (mm):	12.688	12.696	12.514





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N613 B-1 @ 3.05 m - 3.35 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

450

LAB NO:

452

DATE ASSIGNED:

11/4/2013

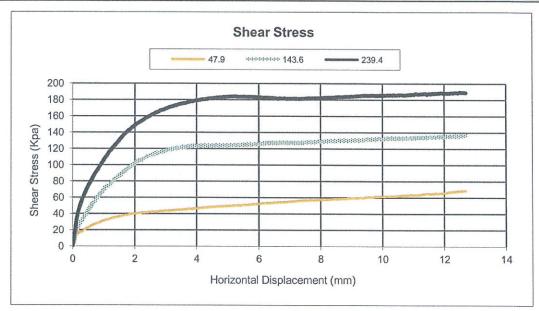
NORMAL LOADS (Kpa):

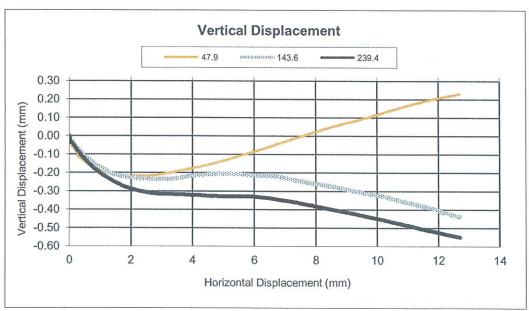
47.9

143.6

239.4

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: SAMPLE PREPARATION: N613 B-3 @ 7.62 m - 7.92 m Insitu-Saturate JOB NO:

1720134030.0002

WORK ORDER NO:

4

LAB NO:

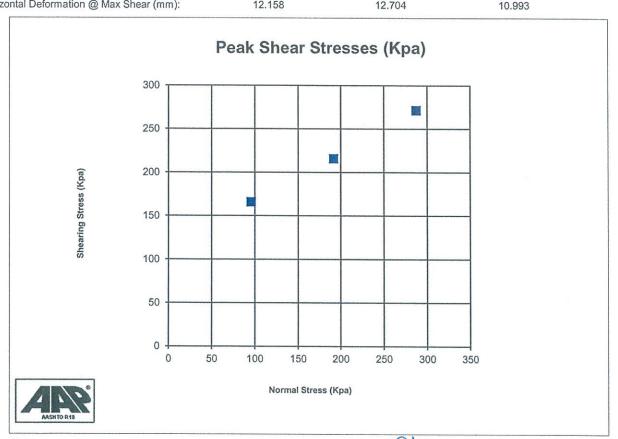
455

DATE ASSIGNED:

11/4/2013

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automated	d Shear Test System by Tra	utwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	95.8	191.5	287.3
Dry mass of specimen (g):	133.8	136.6	141.2
Initial Moisture Content:	18.2%	19.3%	16.4%
Initial Wet Density (Kg per cu.m):	2098.0	2161.1	2179.8
Initial Dry Density (Kg per cu.m):	1775.2	1811.7	1873.0
Final Moisture Content:	18.2%	18.4%	16.5%
Final Wet Density (Kg per cu.m):	2098.3	2143.9	2181.5
Final Dry Density (Kg per cu.m):	1774.4	1810.9	1872.2
Normal Stress (kpa):	95.8	191.5	287.3
Maximum Shearing Stress (Kpa):	165.78	215.69	271.34
Vertical Deformation @ Max Shear (mm):	0.064	-0.181	0.066
Horizontal Deformation @ Max Shear (mm):	12.158	12.704	10.993



REVIEWED BY HULL



BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N613 B-3 @ 7.62 m - 7.92 m

SAMPLE PREPARATION: Insitu-Saturate

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JOB NO:

1720134030.0002

WORK ORDER NO: 4

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LAB NO:

455

DATE ASSIGNED:

11/4/2013

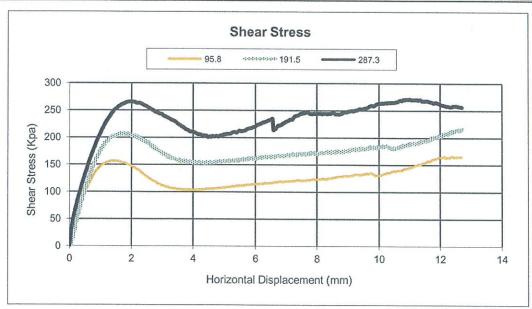
NORMAL LOADS (Kpa):

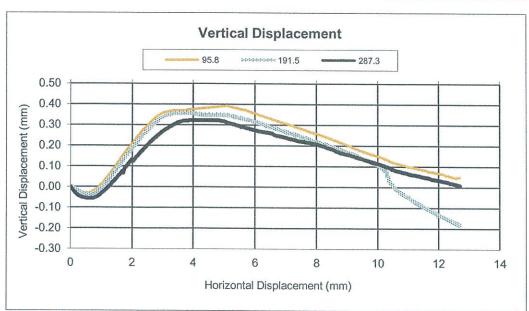
95.8

191.5

287.3

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

Insitu-Saturate

SAMPLE PREPARATION:

SAMPLE SOURCE:

N613 B-3 @ 12.19 m - 12.50 m

JOB NO:

1720134030.0002

WORK ORDER NO:

4

LAB NO:

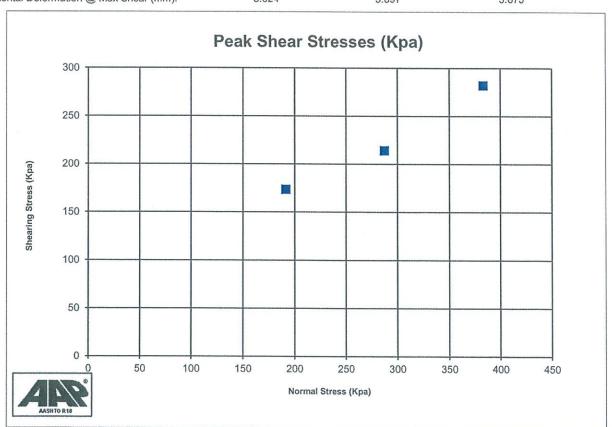
456

DATE ASSIGNED:

11/4/2013

DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automated	d Shear Test System by Tra	utwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	191.5	287.3	383.1
Dry mass of specimen (g):	129.5	126.3	131.1
Initial Moisture Content:	21.1%	22.4%	20.9%
Initial Wet Density (Kg per cu.m):	2078.1	2050.7	2102.8
Initial Dry Density (Kg per cu.m):	1717.4	1675.7	1739.7
Final Moisture Content:	20.4%	21.2%	19.6%
Final Wet Density (Kg per cu.m):	2067.6	2029.7	2079.2
Final Dry Density (Kg per cu.m):	1716.6	1675.0	1738.9
Normal Stress (kpa):	191.5	287.3	383.1
Maximum Shearing Stress (Kpa):	173.57	214.08	282.07
Vertical Deformation @ Max Shear (mm):	-0.245	-0.196	-0.207
Horizontal Deformation @ Max Shear (mm):	8.024	3.697	3.675





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N613 B-3 @ 12.19 m - 12.50 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

456

LAB NO:

100

DATE ASSIGNED:

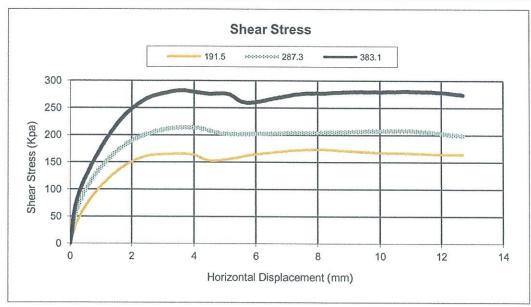
11/4/2013

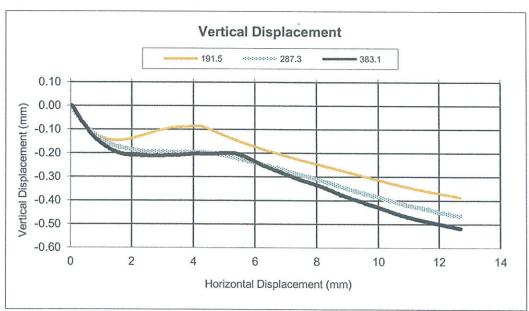
NORMAL LOADS (Kpa):

191.5

287.3

383.1









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N613 B-4 @ 6.10 m - 6.40 m

SAMPLE PREPARATION:

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

4

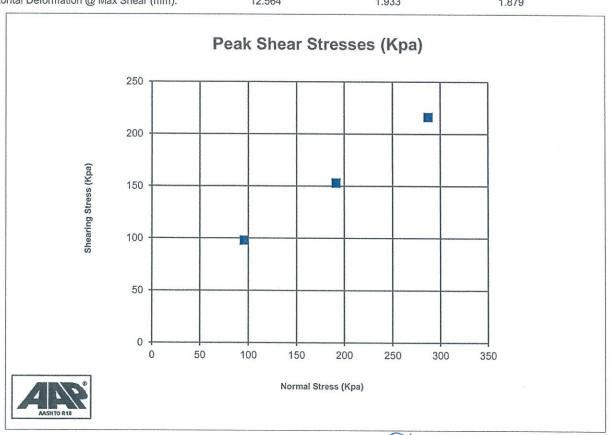
LAB NO:

458

DATE ASSIGNED:

11/4/2013

Initial thickness of specimen (mm):	25.4			
Initial diameter of specimen (mm):	61.5			
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipme	ent
Rate of deformation (mm/min):	0.4064			
Direct shear point (Kpa):	95.8	191.5	287.3	
Dry mass of specimen (g):	129.4	130.5	127.4	
Initial Moisture Content:	21.4%	21.0%	23.0%	
Initial Wet Density (Kg per cu.m):	2083.5	2094.6	2078.5	
Initial Dry Density (Kg per cu.m):	1717.0	1731.5	1690.1	
Final Moisture Content:	21.2%	21.0%	22.5%	
Final Wet Density (Kg per cu.m):	2079.4	2094.0	2068.7	
Initial Dry Density (Kg per cu.m):	1716.2	1730.7	1689.3	
Normal Stress (kpa):	95.8	191.5	287.3	
Maximum Shearing Stress (Kpa):	97.79	152.94	216.16	
Vertical Deformation @ Max Shear (mm):	-0.006	0.166	0.058	
Horizontal Deformation @ Max Shear (mm):	12.564	1.933	1.879	







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N613 B-4 @ 6.10 m - 6.40 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

LAB NO:

458

DATE ASSIGNED:

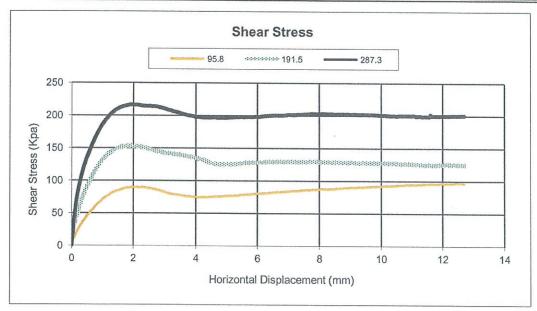
11/4/2013

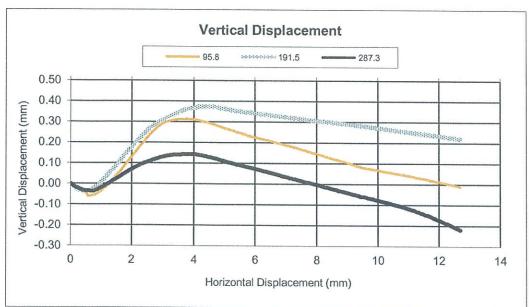
NORMAL LOADS (Kpa):

95.8

191.5

287.3







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: SAMPLE PREPARATION: N614 B-1 @ 6.25 m - 6.55 m

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

4

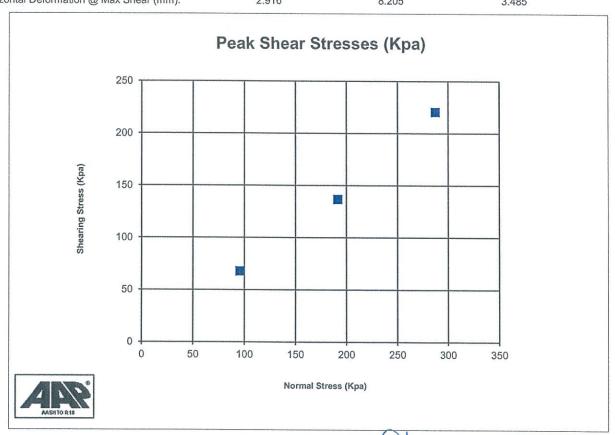
LAB NO:

460

DATE ASSIGNED: 11/4/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	utwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		,
Direct shear point (Kpa):	95.8	191.5	287.3
Dry mass of specimen (g):	123.4	128.0	127.8
Initial Moisture Content:	23.6%	21.9%	21.6%
Initial Wet Density (Kg per cu.m):	2023.1	2068.4	2060.1
Initial Dry Density (Kg per cu.m):	1637.5	1697.8	1695.5
Final Moisture Content:	28.2%	22.6%	21.7%
Final Wet Density (Kg per cu.m):	2098.5	2080.5	2062.5
Final Dry Density (Kg per cu.m):	1636.8	1697.0	1694.7
Normal Stress (kpa):	95.8	191.5	287.3
Maximum Shearing Stress (Kpa):	67.76	136.62	220.45
Vertical Deformation @ Max Shear (mm):	-0.049	-0.094	-0.058
Horizontal Deformation @ Max Shear (mm):	2.916	8.205	3.485





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N614 B-1 @ 6.25 m - 6.55 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

460

LAB NO: DATE ASSIGNED:

11/4/2013

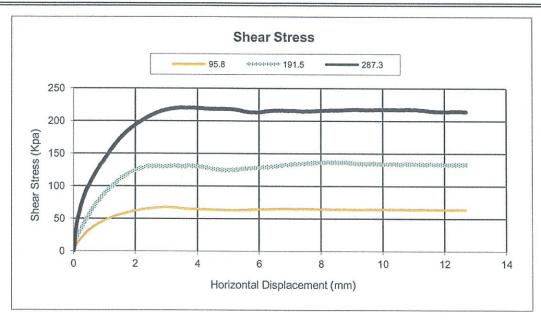
NORMAL LOADS (Kpa):

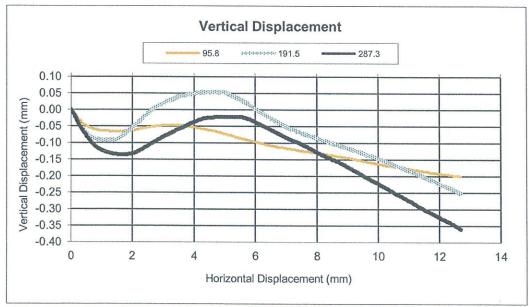
95.8

191.5

287.3

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: SAMPLE PREPARATION: N614 B-2 @ 10.67 m- 10.97 m

Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO:

DATE ASSIGNED:

4

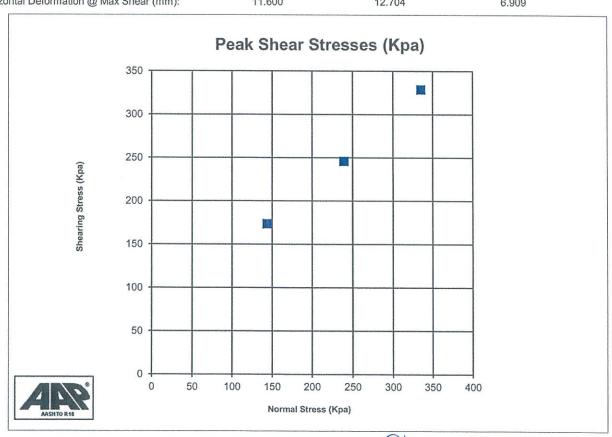
LAB NO:

463

11/4/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4		
Initial diameter of specimen (mm):	61.5		
Shearing device used:	DigiShear Automate	d Shear Test System by Tra	autwein Soil Testing Equipment
Rate of deformation (mm/min):	0.4064		
Direct shear point (Kpa):	143.6	239.4	335.2
Dry mass of specimen (g):	145.1	144.2	145.9
Initial Moisture Content:	13.6%	14.1%	14.0%
Initial Wet Density (Kg per cu.m):	2187.1	2180.7	2205.0
Initial Dry Density (Kg per cu.m):	1925.6	1912.8	1935.4
Final Moisture Content:	15.5%	15.9%	15.6%
Final Wet Density (Kg per cu.m):	2223.2	2216.3	2236.4
Final Dry Density (Kg per cu.m):	1924.7	1911.9	1934.5
Normal Stress (kpa):	143.6	239.4	335.2
Maximum Shearing Stress (Kpa):	173.45	245.85	328.59
Vertical Deformation @ Max Shear (mm):	-0.036	-0.006	0.153
Horizontal Deformation @ Max Shear (mm):	11.600	12.704	6.909





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N614 B-2 @ 10.67 m- 10.97 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

. 4

LAB NO:

463

DATE ASSIGNED:

11/4/2013

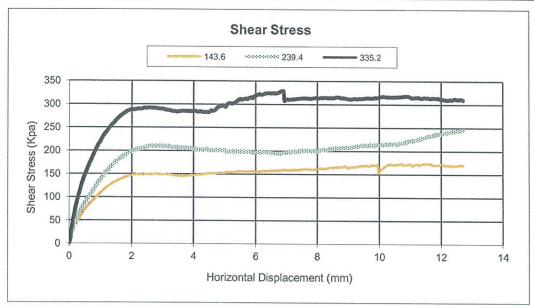
NORMAL LOADS (Kpa):

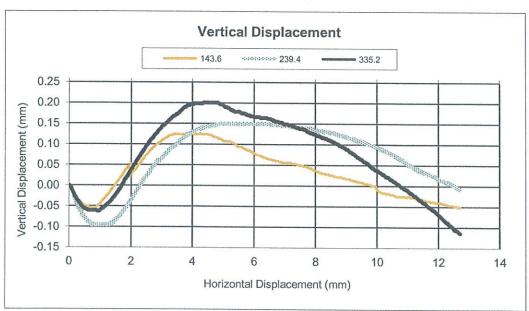
143.6

239.4

335.2

### DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)





Oly



BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: SAMPLE PREPARATION: N614 B-4 @ 3.05 m - 3.35 m

Insitu-Saturate

JOB NO:

WORK ORDER NO:

4

LAB NO:

464

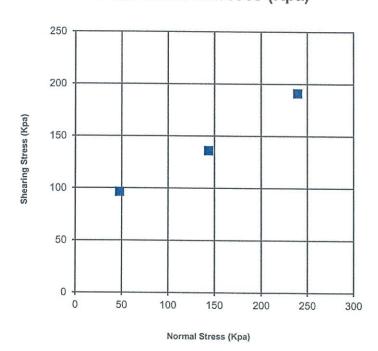
DATE ASSIGNED:

11/4/2013

# DIRECT SHEAR TEST OF SOILS UNDER CONSOLIDATED DRAINED CONDITIONS (AASHTO T-236)

Initial thickness of specimen (mm):	25.4			
Initial diameter of specimen (mm):	61.5			
Shearing device used:	DigiShear Automated Shear Test System by Trautwein Soil Testing Equipment			
Rate of deformation (mm/min):	0.4064			
Direct shear point (Kpa):	47.9	143.6	239.4	
Dry mass of specimen (g):	140.3	138.8	141.0	
Initial Moisture Content:	8.8%	10.5%	10.3%	
Initial Wet Density (Kg per cu.m):	2025.1	2033.9	2062.5	
Initial Dry Density (Kg per cu.m):	1861.3	1841.0	1870.4	
Final Moisture Content:	21.5%	21.5%	19.2%	
Final Wet Density (Kg per cu.m):	2260.2	2236.7	2228.9	
Final Dry Density (Kg per cu.m):	1860.5	1840.2	1869.5	
Normal Stress (kpa):	47.9	143.6	239.4	
Maximum Shearing Stress (Kpa):	96.33	135.95	190.93	
Vertical Deformation @ Max Shear (mm):	0.335	-0.038	-0.621	
Horizontal Deformation @ Max Shear (mm):	12.704	12.704	12.575	

# Peak Shear Stresses (Kpa)







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE:

N614 B-4 @ 3.05 m - 3.35 m

SAMPLE PREPARATION: Insitu-Saturate

JOB NO:

1720134030.0002

WORK ORDER NO: 4

464

LAB NO: DATE ASSIGNED:

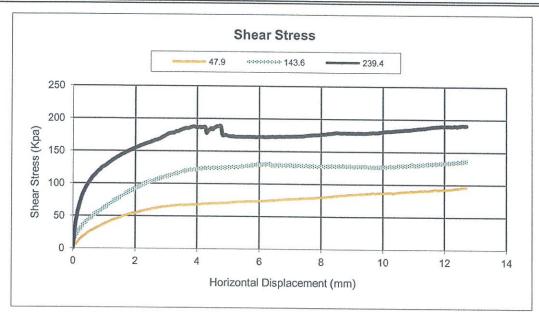
11/4/2013

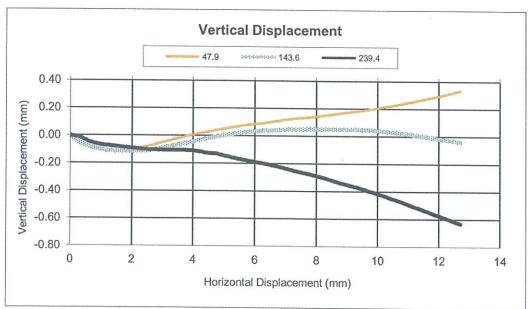
NORMAL LOADS (Kpa):

47.9

143.6

239.4







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE PREP: INSITU

**SAMPLE SOURCE:** N503 B-1 10.52 m - 10.67 m

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

**DATE SAMPLED: 11/06/13** 

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL **APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.00 cm

MAXIMUM STRESS:

25,249 KPa

HEIGHT:

14.02 cm

AT STRAIN:

4.26%

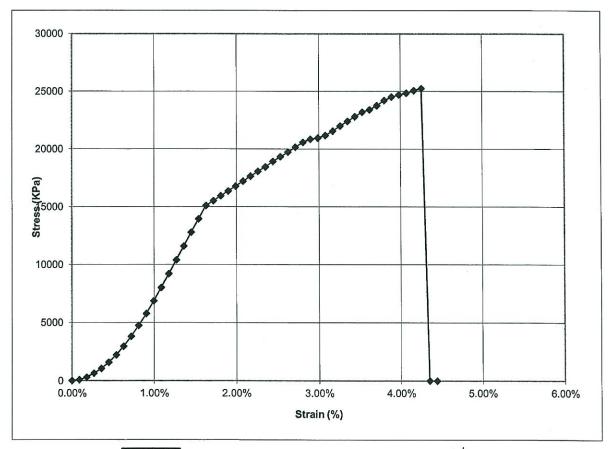
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,152.4 kg/cu.m

L/D (2.0-2.5 REQ.):

2.34

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N503 B-1 13.72 m - 13.94 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

464

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.00 cm

MAXIMUM STRESS:

AT STRAIN:

30,100 KPa

3.38%

HEIGHT:

14.27 cm

5.1% cm/min.

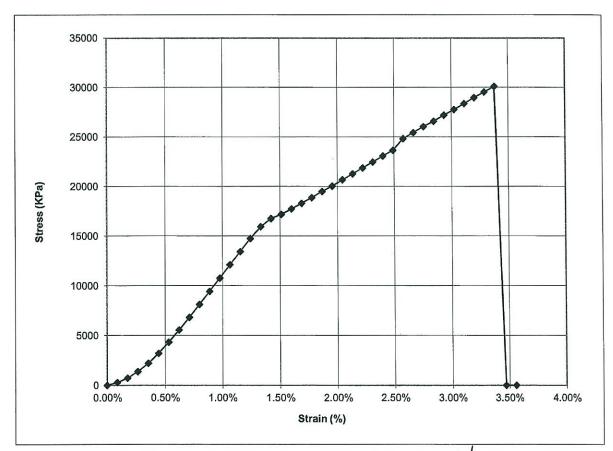
STRAIN RATE: DRY DENSITY:

2,470.5 kg/cu.m

L/D (2.0-2.5 REQ.):

2.38

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N503 B-2 @ 15.39 m - 15.58 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

466

DATE SAMPLED: 11/06/13

## UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

5.99 cm

MAXIMUM STRESS:

AT STRAIN:

12,844 KPa

HEIGHT:

13.89 cm

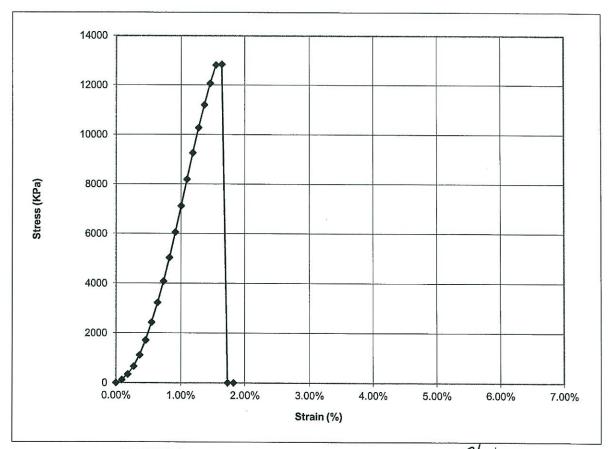
1.65%

STRAIN RATE: DRY DENSITY: 5.1% cm/min. 2,445.0 kg/cu.m

L/D (2.0-2.5 REQ.):

2.32

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N503 B-3 @ 4.57 m - 4.88 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 4

LAB NO:

449

DATE SAMPLED: 11/04/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.12 cm

MAXIMUM STRESS:

18 KPa

HEIGHT:

15.21 cm

AT STRAIN:

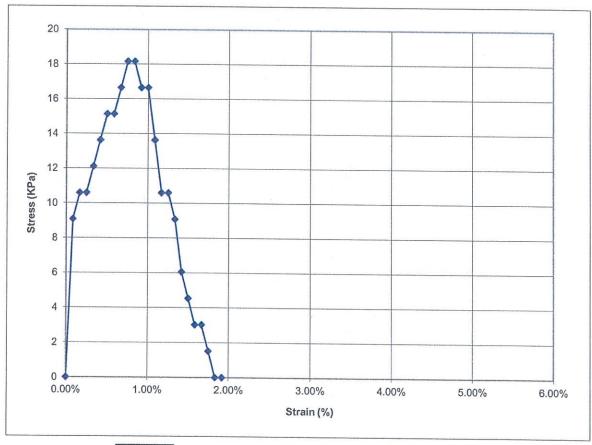
0.75%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

L/D (2.0-2.5 REQ.):

1,927.7 kg/cu.m 2.49

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N503 B-3 @ 12.53 m - 12.65 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

5.59 cm

MAXIMUM STRESS:

18,623 KPa

HEIGHT:

12.83 cm

AT STRAIN:

2.08%

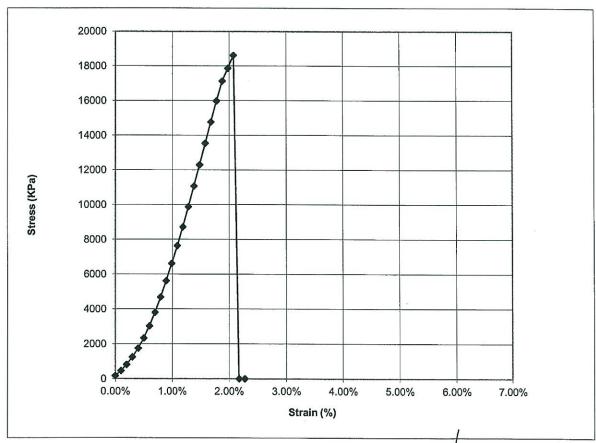
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,197.8 kg/cu.m

L/D (2.0-2.5 REQ.):

2.29

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N503 B-3 @ 16.49 m - 16.64 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

468

LAB NO:

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

5.70 cm

MAXIMUM STRESS:

40,142 KPa

HEIGHT:

13.67 cm

AT STRAIN:

4.18%

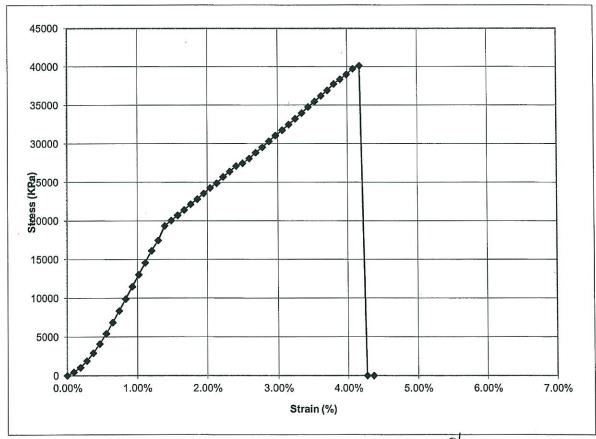
STRAIN RATE: DRY DENSITY: 5.1% cm/min.

2,463.2 kg/cu.m

L/D (2.0-2.5 REQ.):

2.40

### SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N503 B-4 @ 13.38 m - 13.53 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

469

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

5.96 cm

MAXIMUM STRESS:

31,202 KPa

HEIGHT:

13.53 cm

AT STRAIN:

4.97%

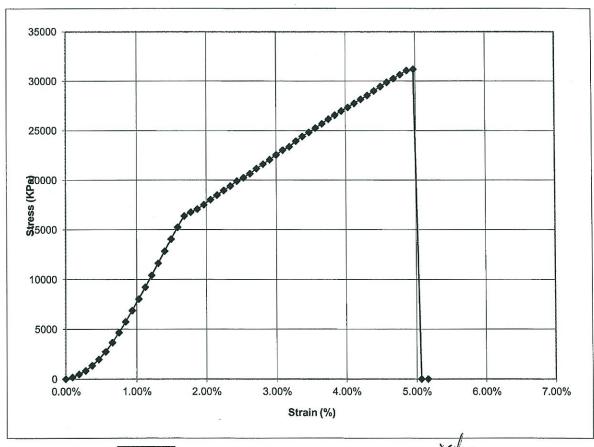
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,411.5 kg/cu.m

L/D (2.0-2.5 REQ.):

2.27

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N503 B-4 @ 15.79 m - 15.85 m

SAMPLE PREP: INSITU JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

470

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.04 cm

MAXIMUM STRESS:

AT STRAIN:

32,531 KPa

3.90%

HEIGHT:

13.66 cm

5.1% cm/min.

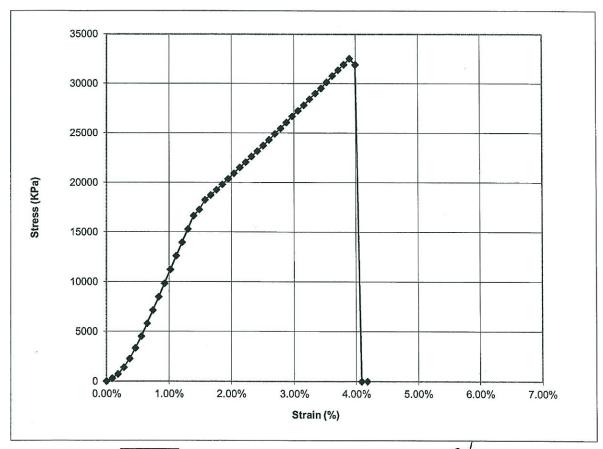
STRAIN RATE: DRY DENSITY:

2,441.5 kg/cu.m

L/D (2.0-2.5 REQ.):

2.26

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL: SAMPLE SOURCE: N504 B-2; 9.30 m - 9.60 m

Bore hole samples

SAMPLE PREP:

INSITU

JOB NO:

1720134030.0002

WORK ORDER 3

LAB NO:

317 **DATE SAMPLE 10/02/13** 

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.13 cm

MAXIMUM STRESS:

AT STRAIN:

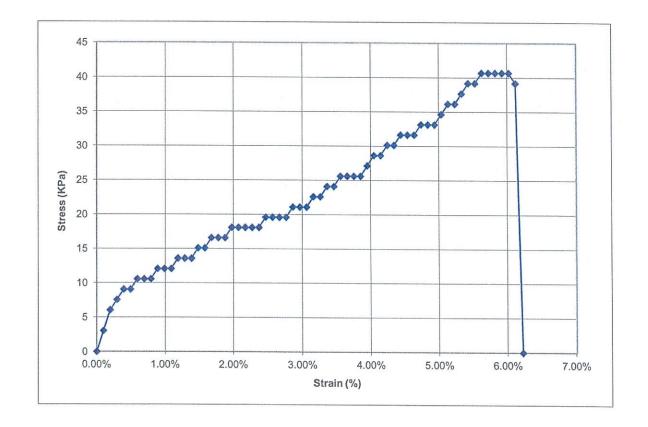
41 KPa

HEIGHT: STRAIN RATE: 12.87 cm 5.1% cm/min.

5.62%

DRY DENSITY:

1,741.3 kg/cu.m







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N504 B-3; 14.48 m - 14.78 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030.0002

WORK ORDER NO: 3

LAB NO:

DATE SAMPLED: 10/02/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.15 cm

MAXIMUM STRESS:

6 KPa

HEIGHT:

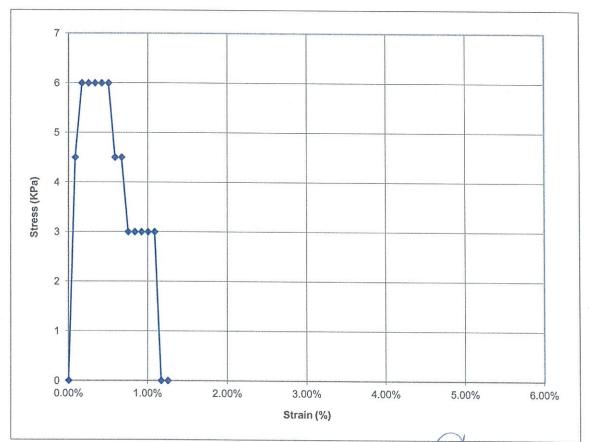
15.19 cm

AT STRAIN:

0.25%

STRAIN RATE: DRY DENSITY:

5.1% cm/min. 1,859.4 kg/cu.m





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N505 B-1 @ 6.54 m - 6.71 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

486

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER: HEIGHT:

5.92 cm

MAXIMUM STRESS:

43,733 KPa

STRAIN RATE:

12.70 cm

AT STRAIN:

3.00%

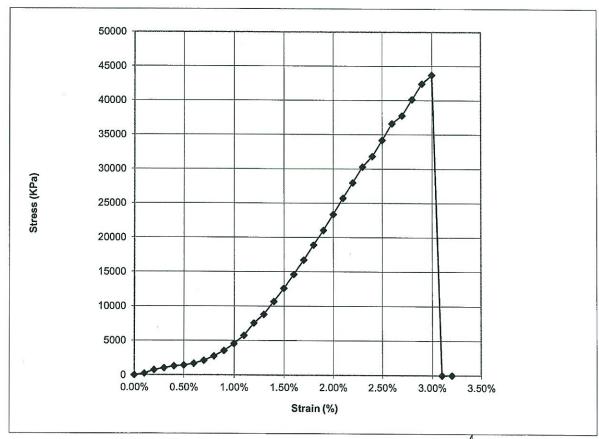
DRY DENSITY:

5.1% cm/min. 2,082.2 kg/cu.m

L/D (2.0-2.5 REQ.):

2.15

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N505 B-1 @ 10.36 m - 10.55 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

487

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL **APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.00 cm

MAXIMUM STRESS:

40,539 KPa

HEIGHT:

12.45 cm

AT STRAIN:

2.55%

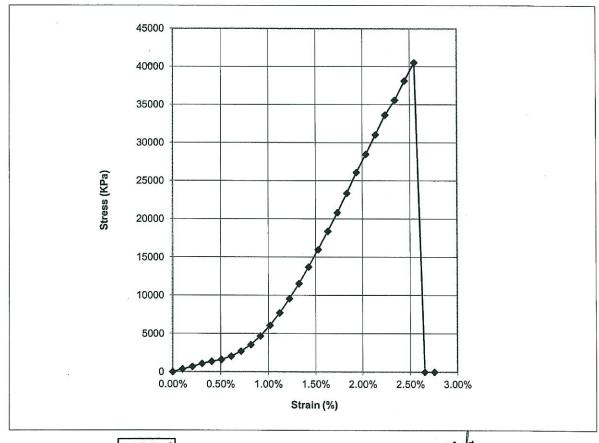
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,114.1 kg/cu.m

L/D (2.0-2.5 REQ.):

2.07

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N505 B-2 @ 11.70 m - 11.90 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

488

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL** APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.00 cm

MAXIMUM STRESS:

39,061 KPa

HEIGHT:

13.27 cm

AT STRAIN:

2.39%

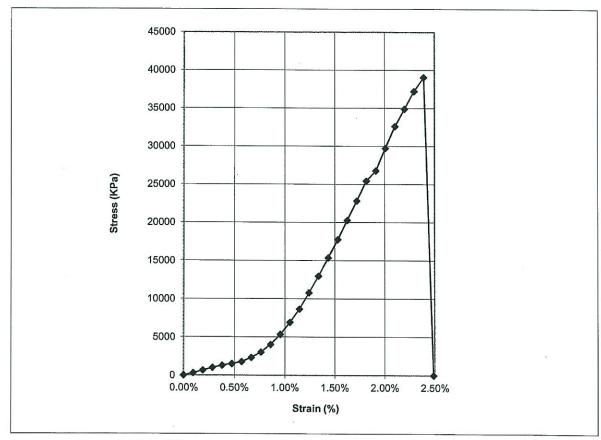
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,098.1 kg/cu.m

L/D (2.0-2.5 REQ.):

2.21

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N505 B-2 @ 13.38 m - 13.53 m

SAMPLE PREP: INSITU JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

489

DATE SAMPLED:

11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.02 cm

MAXIMUM STRESS:

33,827 KPa

HEIGHT:

12.80 cm

AT STRAIN:

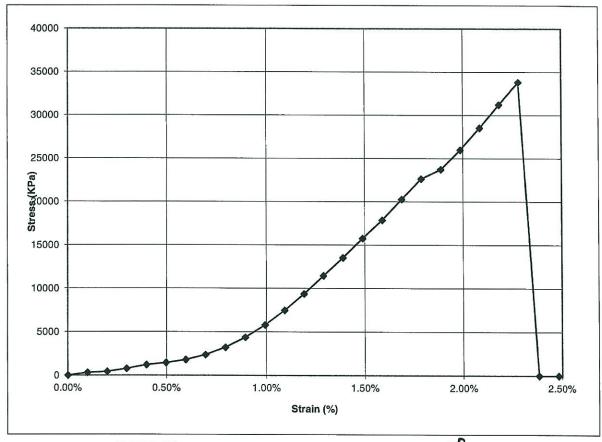
2.28%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

2,102.6 kg/cu.m

L/D (2.0-2.5 REQ.): 2.13

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N505 B-3 @ 6.22 m - 6.43 m

SAMPLE PREP: INSITU JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO: 490

DATE SAMPLED:

11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

5.99 cm

MAXIMUM STRESS:

42,314 KPa

HEIGHT:

13.43 cm

AT STRAIN:

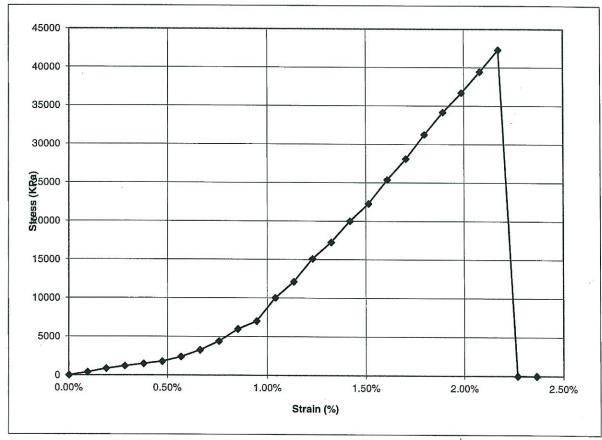
2.17%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

2,117.3 kg/cu.m

L/D (2.0-2.5 REQ.): 2.24







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N505 B-3 @ 10.47 m - 10.61 m

SAMPLE PREP: INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

491

DATE SAMPLED:

11/06/13

# UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.04 cm

MAXIMUM STRESS:

24,694 KPa

HEIGHT:

12.86 cm

AT STRAIN:

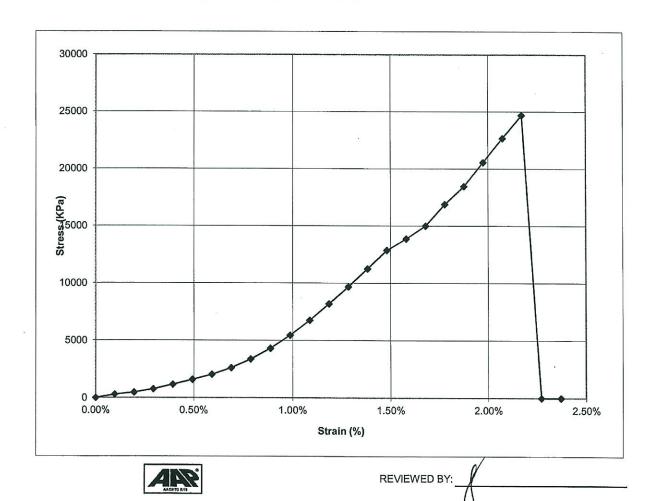
2.17%

STRAIN RATE: DRY DENSITY: 5.1% cm/min. 2,057.7 kg/cu.m

L/D (2.0-2.5 REQ.):

2.13

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA-N12 Bridges Navajo, NM to Junction N64 AZ

LOCATION:

NM to Junction N64 AZ

MATERIAL:

Bore hole samples SAMPLE SOURCE: N505 B-4 @ 9.02 m - 9.17 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

493

LAB NO: DATE SAMPLED:

11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL** APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.08 cm

MAXIMUM STRESS:

37,604 KPa

HEIGHT:

12.00 cm

AT STRAIN:

2.12%

STRAIN RATE: DRY DENSITY:

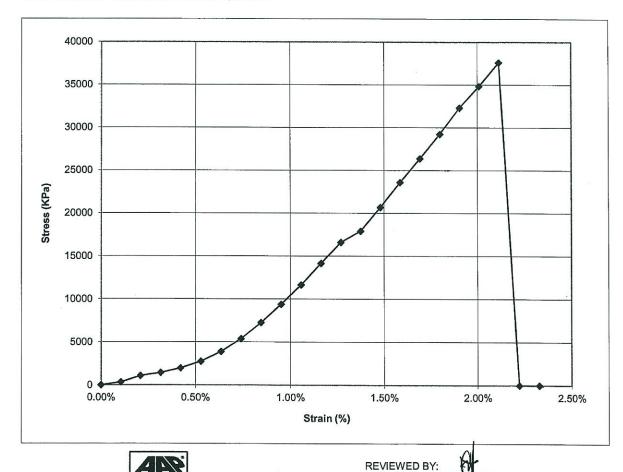
5.1% cm/min. 2,069.6 kg/cu.m

L/D (2.0-2.5 REQ.):

1.97

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N613 B-1 @ 10.45 m - 10.61 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

479

DATE SAMPLED: 11/06/13

# UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.01 cm

MAXIMUM STRESS:

AT STRAIN:

6,921 KPa

1.83%

HEIGHT:

12.48 cm

5.1% cm/min.

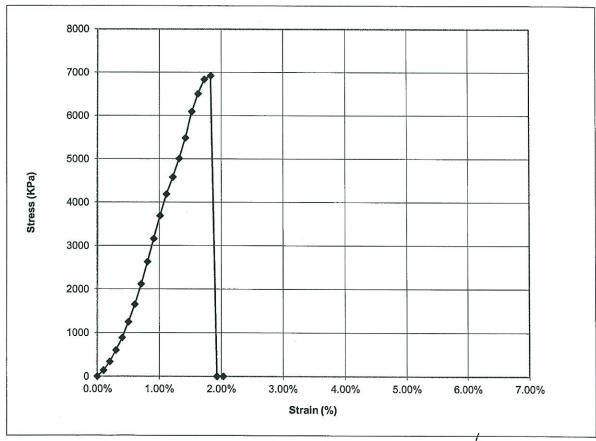
STRAIN RATE: DRY DENSITY:

2,395.5 kg/cu.m

L/D (2.0-2.5 REQ.):

2.07

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST



AN.





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N613 B-1 @ 13.20 m - 13.35 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO** 5

LAB NO:

480

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL** APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.03 cm

MAXIMUM STRESS:

16,986 KPa

HEIGHT:

14.56 cm

AT STRAIN:

1.74%

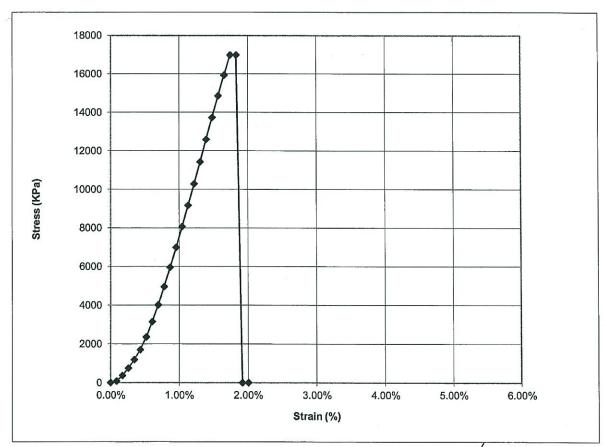
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,449.1 kg/cu.m

L/D (2.0-2.5 REQ.):

2.42

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N613 B-2 @ 10.70 m -10.82 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO: DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMENS (AASHTO T208-10) as applicable

DIAMETER:

6.00 cm

11.15 cm

MAXIMUM STRESS:

AT STRAIN:

6,040 KPa

2.39%

HEIGHT: STRAIN RATE:

5.1% cm/min.

DRY DENSITY:

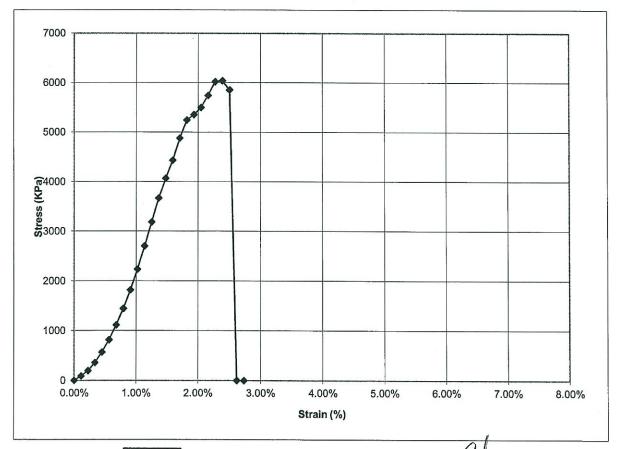
2,313.1 kg/cu.m

L/D (2.0-2.5 REQ.):

1.86

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N613 B-2 @ 12.98 m -13.20 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

482

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.06 cm

MAXIMUM STRESS:

15,997 KPa

HEIGHT:

14.39 cm

AT STRAIN:

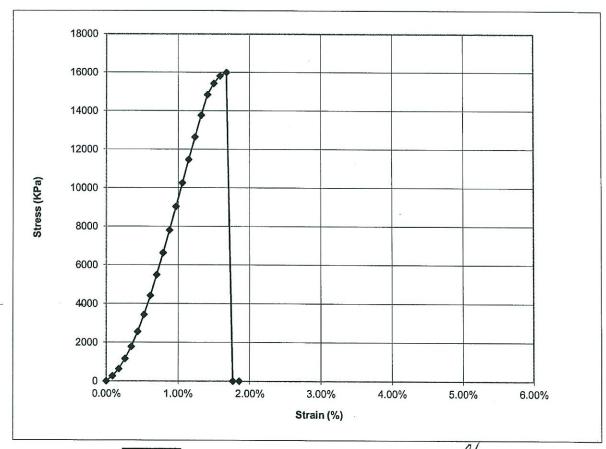
1.68%

STRAIN RATE: DRY DENSITY: 5.1% cm/min. 2,404.3 kg/cu.m

L/D (2.0-2.5 REQ.):

2.37

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST



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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N613 B-3 @ 19.78 m - 19.93 m

SAMPLE PREP: INSITU JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL** APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

5.93 cm

MAXIMUM STRESS:

6,049 KPa

**HEIGHT:** 

13.96 cm

AT STRAIN:

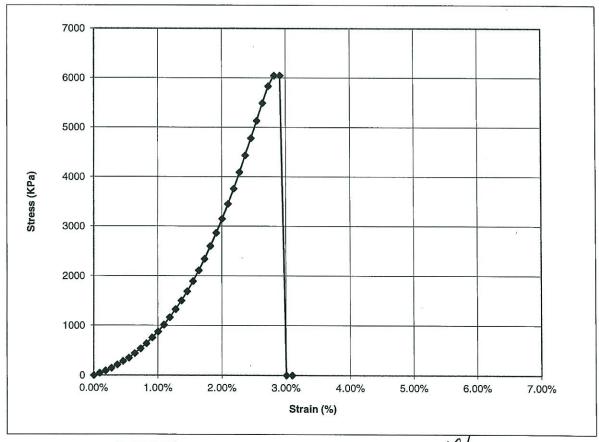
2.91%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

L/D (2.0-2.5 REQ.):

2,190.9 kg/cu.m 2.35

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST









BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N613 B-4 @ 12.86 m - 13.01 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

484

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.01 cm

MAXIMUM STRESS:

18,325 KPa

HEIGHT:

12.19 cm

AT STRAIN:

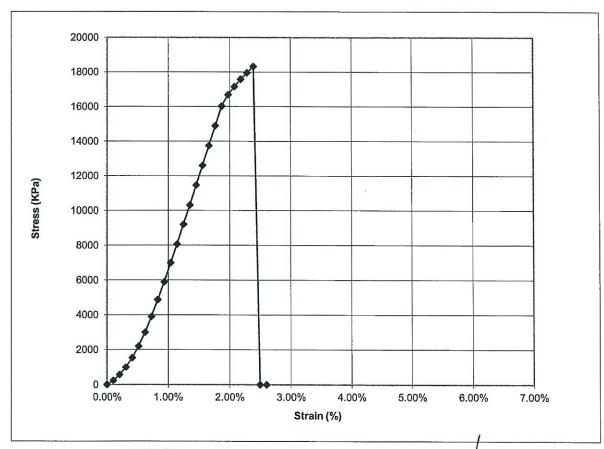
2.40%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

L/D (2.0-2.5 REQ.):

2,437.9 kg/cu.m 2.03

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N613 B-4 @ 15.15 m - 15.32 m SAMPLE PREP:

INSITU

JOB NO:

1720134030

WORK ORDER NO: 5

LAB NO:

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL** APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.01 cm

MAXIMUM STRESS:

12,018 KPa

HEIGHT:

12.03 cm

AT STRAIN:

2.53%

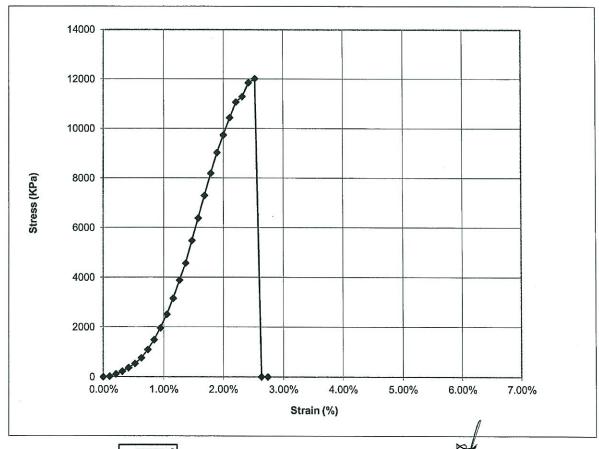
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,398.6 kg/cu.m

L/D (2.0-2.5 REQ.):

2.00

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N614 B-1 @ 13.90 m - 14.02 m SAMPLE PREP: INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

471

LAB NO: DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL **APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.05 cm

MAXIMUM STRESS:

7,445 KPa

**HEIGHT:** 

11.93 cm

AT STRAIN:

2.24%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

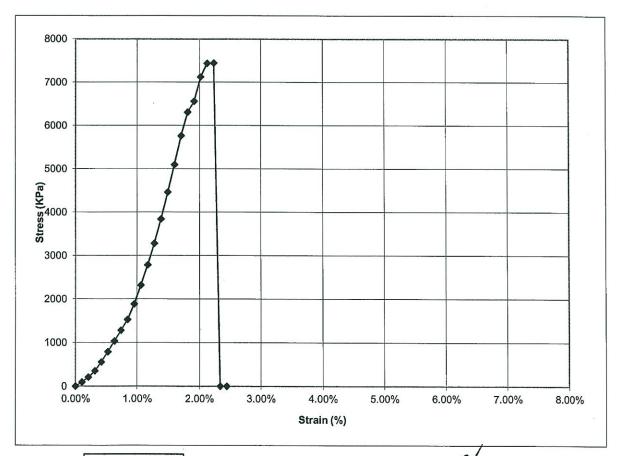
2,142.1 kg/cu.m

L/D (2.0-2.5 REQ.):

1.97

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N614 B-1 @ 17.10 m - 17.22 m

SAMPLE PREP: INSITU JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

472

DATE SAMPLED: 11/06/13

### UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.08 cm

MAXIMUM STRESS:

18,795 KPa

HEIGHT:

11.66 cm

AT STRAIN:

2.18%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

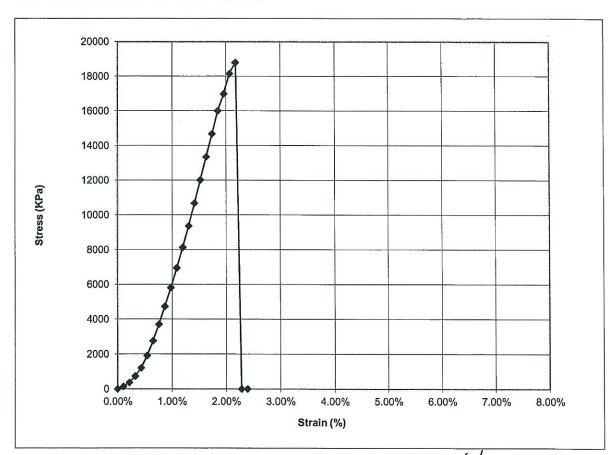
2,491.1 kg/cu.m

L/D (2.0-2.5 REQ.):

1.92

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

**SAMPLE SOURCE:** N614 B-2 @ 13.11 m - 13.26 m SAMPLE PREP: INSITU

Bore hole samples

JOB NO:

1720134030

WORK ORDER NO: 5 LAB NO:

473

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.07 cm

MAXIMUM STRESS:

10,887 KPa

HEIGHT:

11.01 cm

AT STRAIN:

2.54%

STRAIN RATE:

5.1% cm/min.

DRY DENSITY:

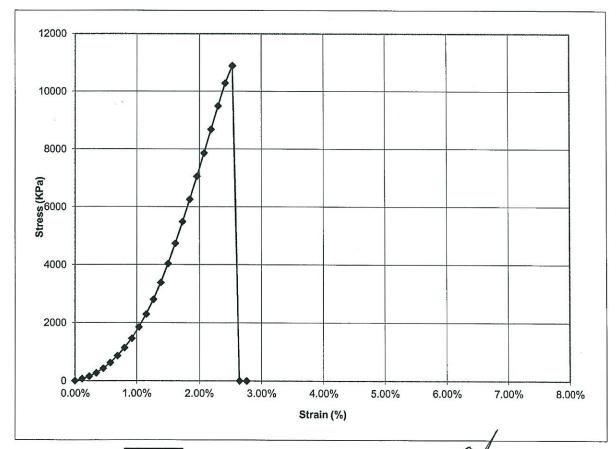
2,187.4 kg/cu.m

L/D (2.0-2.5 REQ.):

1.81

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE PREP:

**SAMPLE SOURCE:** N614 B-2 @ 16.22 m - 16.34 m

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.09 cm

MAXIMUM STRESS:

14,321 KPa

HEIGHT:

11.73 cm

AT STRAIN:

2.60%

STRAIN RATE: DRY DENSITY:

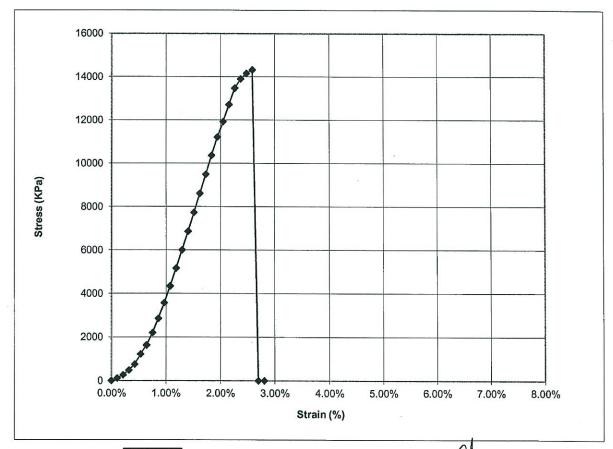
5.1% cm/min. 2,266.4 kg/cu.m

L/D (2.0-2.5 REQ.):

1.93

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.







BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL: SAMPLE SOURCE: N614 B-3 @ 9.85 m - 10.00 m

Bore hole samples

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO: 5** 

LAB NO:

475

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)**

DIAMETER:

6.09 cm

MAXIMUM STRESS:

12,149 KPa

HEIGHT:

12.34 cm

AT STRAIN:

2.16%

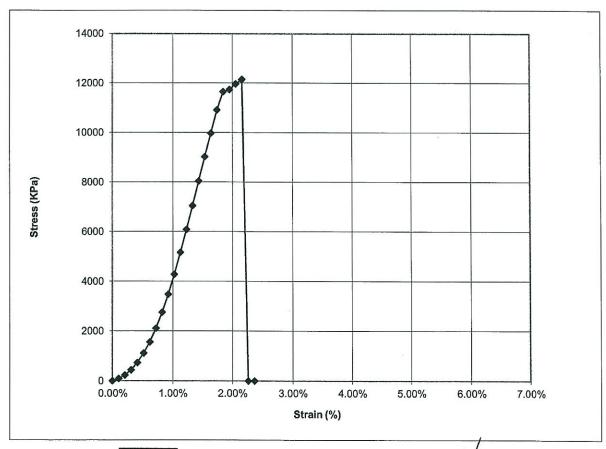
STRAIN RATE: DRY DENSITY:

5.1% cm/min. 2,157.1 kg/cu.m

L/D (2.0-2.5 REQ.):

2.03

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N614 B-3 @ 11.89 m - 12.01 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO** 5

AD NO.

**LAB NO**: 476

DATE SAMPLED: 11/06/13

# UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.08 cm

MAXIMUM STRESS:

15,093 KPa

HEIGHT:

11.23 cm

AT STRAIN:

2.15%

STRAIN RATE:

5.1% cm/min.

DRY DENSITY:

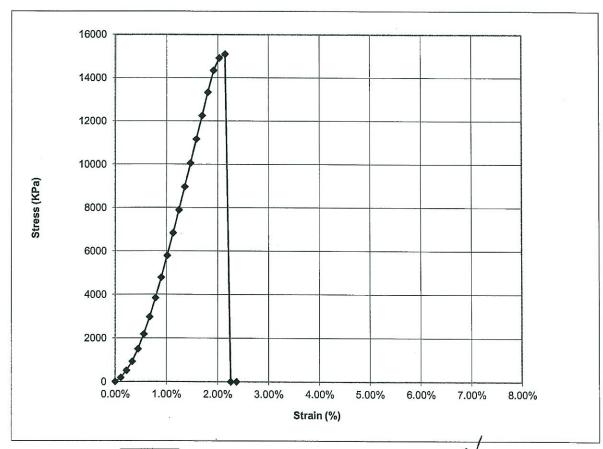
2,214.5 kg/cu.m

L/D (2.0-2.5 REQ.):

1.85

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST

Note: The L/D did not satisfy the 2.0 to 2.5 requirement.



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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N614 B-4 @ 13.44 m - 13.66 m

SAMPLE PREP:

INSITU

JOB NO:

1720134030

**WORK ORDER NO** 5

LAB NO:

DATE SAMPLED: 11/06/13

### **UNCONFINED COMPRESSION STRENGTH OF COHESIVE SOIL** APPLICABLE PORTIONS OF (AASHTO T208-10)

DIAMETER:

6.08 cm

MAXIMUM STRESS:

9,758 KPa

HEIGHT:

15.04 cm

AT STRAIN:

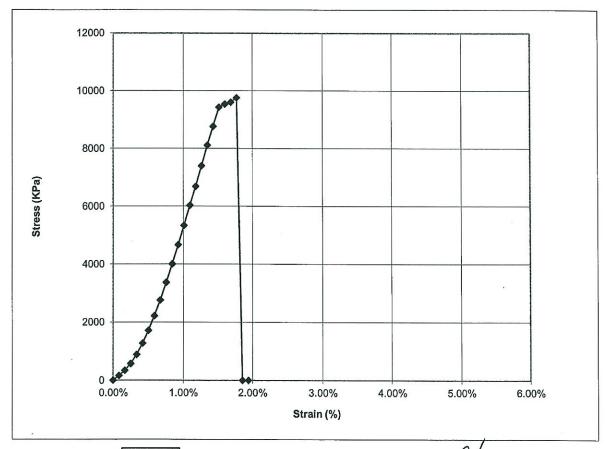
1.77%

STRAIN RATE: DRY DENSITY: 5.1% cm/min.

L/D (2.0-2.5 REQ.):

2,205.1 kg/cu.m 2.47

SPECIMEN CONTAINED IN A SEALED PLASTIC BAG UNTIL TIME OF TEST





BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE**: N503 B-2 @ 4.57 m - 4.88 m

SAMPLE PREP:

Undisturbed Saturate at 191 Kpa JOB NO:

1720134030.0002

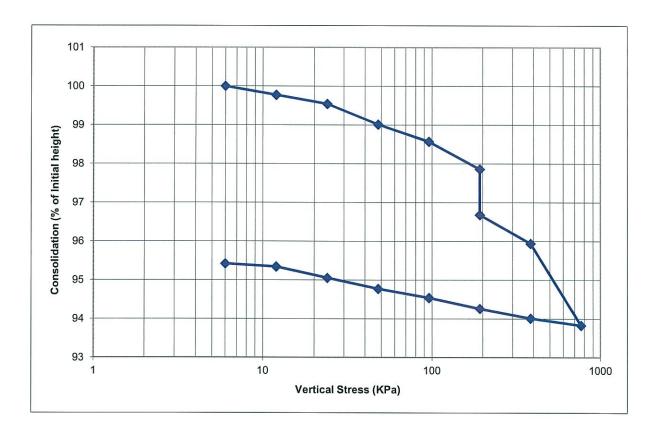
**WORK ORDER NO: 4** LAB NO:

446

DATE SAMPLED: 11/4/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.37	FINAL VOLUME (cu.cm)	70.72
INITIAL MOISTURE CONTENT	10.2%	FINAL MOISTURE CONTENT	13.1%
INITIAL DRY DENSITY (kg per cu.m)	1854.7	FINAL DRY DENSITY (kg per cu.m)	1969.3
INITIAL DEGREE OF SATURATION	62%	FINAL DEGREE OF SATURATION	100%
INITIAL VOID RATIO	0.44	FINAL VOID RATIO	0.35
ESTIMATED SPECIFIC GRAVITY	2.660	SATURATED AT	191.57 KPa







BIA project N12(12-2)(19-2)2+4 Navajo, NM to N64 junction AZ (near Tsaile, AZ) LOCATION:

MATERIAL: Bore hole samples

**SAMPLE SOURCE**: N503 B-4 @ 3.05 m - 3.35 m SAMPLE PREP: Undisturbed

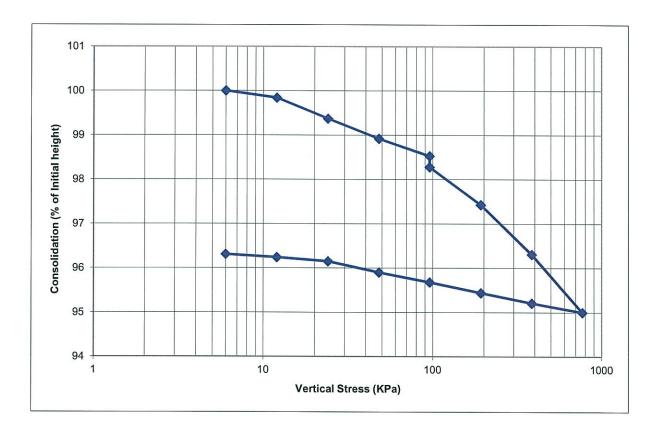
Saturate at 96 Kpa

JOB NO: 1720134030.0002

**WORK ORDER NO: 4** LAB NO: 450 DATE SAMPLED: 11/4/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.37	FINAL VOLUME (cu.cm)	71.61
INITIAL MOISTURE CONTENT	10.4%	FINAL MOISTURE CONTENT	12.4%
INITIAL DRY DENSITY (kg per cu.m)	1884.8	FINAL DRY DENSITY (kg per cu.m)	1976.6
INITIAL DEGREE OF SATURATION	70%	FINAL DEGREE OF SATURATION	100%
INITIAL VOID RATIO	0.39	FINAL VOID RATIO	0.32
ESTIMATED SPECIFIC GRAVITY	2.620	SATURATED AT	95.785 KPa





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples **SAMPLE SOURCE**: N504 B-1; 2.44 m - 2.74 m

SAMPLE PREP:

Undisturbed

Saturate at 96 Kpa

JOB NO:

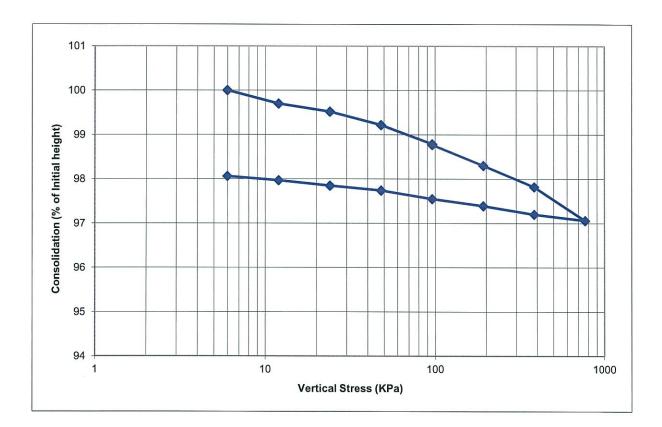
1720134030.0002

**WORK ORDER N(3** LAB NO:

310 DATE SAMPLED: 10/2/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.38	FINAL VOLUME (cu.cm)	73.16
INITIAL MOISTURE CONTENT	10.9%	FINAL MOISTURE CONTENT	11.4%
INITIAL DRY DENSITY (kg per cu.m)	1911.5	FINAL DRY DENSITY (kg per cu.m)	1961.8
INITIAL DEGREE OF SATURATION	82%	FINAL DEGREE OF SATURATION	95%
INITIAL VOID RATIO	0.35	FINAL VOID RATIO	0.31
ESTIMATED SPECIFIC GRAVITY	2.570	SATURATED AT	95.785 KPa





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE**: N504 B-4; 4.72 m - 5.03 m SAMPLE PREP:

Undisturbed

Saturate at 191 Kpa

JOB NO:

1720134030.0002

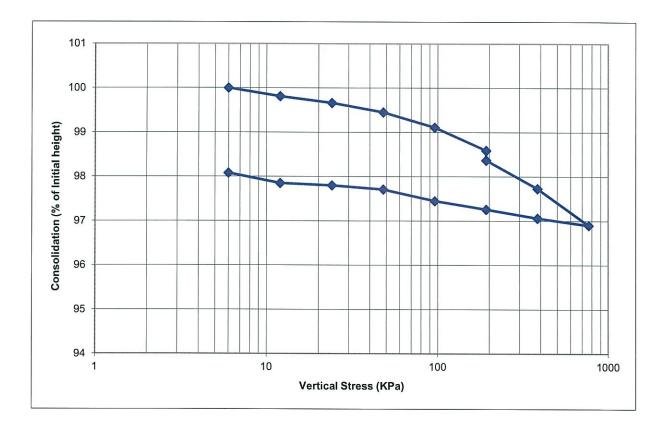
**WORK ORDER NO** 3

LAB NO:

328 DATE SAMPLED: 10/2/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.38	FINAL VOLUME (cu.cm)	73.04
INITIAL MOISTURE CONTENT	8.4%	FINAL MOISTURE CONTENT	11.0%
INITIAL DRY DENSITY (kg per cu.m)	1961.5	FINAL DRY DENSITY (kg per cu.m)	2016.5
INITIAL DEGREE OF SATURATION	65%	FINAL DEGREE OF SATURATION	95%
INITIAL VOID RATIO	0.35	FINAL VOID RATIO	0.30
ESTIMATED SPECIFIC GRAVITY	2.630	SATURATED AT	191.57 KPa





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE**: N613 B-3 @ 3.05 m - 3.35 m

SAMPLE PREP: Undisturbed

Saturate at 96 Kpa

JOB NO:

1720134030.0002

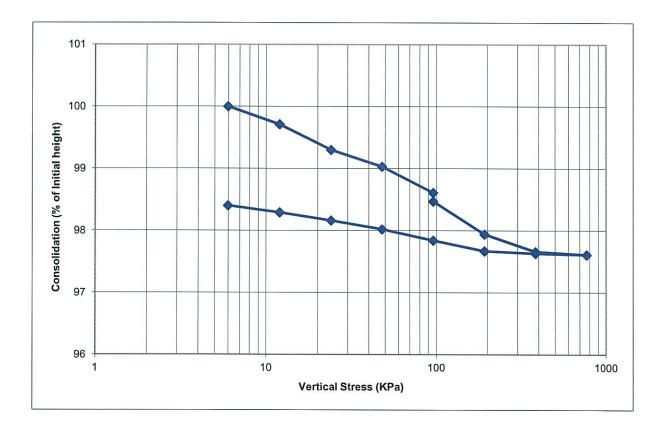
LAB NO:

**WORK ORDER NO: 4** 454

DATE SAMPLED: 11/4/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.37	FINAL VOLUME (cu.cm)	73.57
INITIAL MOISTURE CONTENT	9.1%	FINAL MOISTURE CONTENT	13.4%
INITIAL DRY DENSITY (kg per cu.m)	1797.0	FINAL DRY DENSITY (kg per cu.m)	1834.0
INITIAL DEGREE OF SATURATION	63%	FINAL DEGREE OF SATURATION	100%
INITIAL VOID RATIO	0.36	FINAL VOID RATIO	0.32
ESTIMATED SPECIFIC GRAVITY	2.429	SATURATED AT	95.785 KPa





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE**: N613 B-4 @ 3.05 m - 3.35 m

SAMPLE PREP:

Undisturbed Saturate at 96 Kpa JOB NO:

1720134030.0002

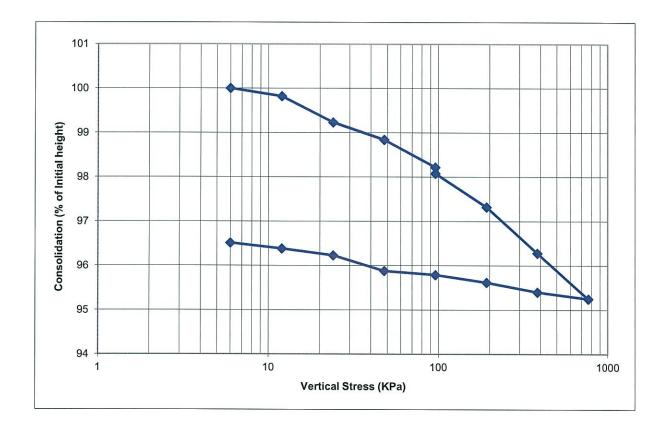
LAB NO:

WORK ORDER NO: 4 457

DATE SAMPLED: 11/4/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.37	FINAL VOLUME (cu.cm)	71.79
INITIAL MOISTURE CONTENT	12.6%	FINAL MOISTURE CONTENT	14.8%
INITIAL DRY DENSITY (kg per cu.m)	1763.3	FINAL DRY DENSITY (kg per cu.m)	1844.3
INITIAL DEGREE OF SATURATION	73%	FINAL DEGREE OF SATURATION	100%
INITIAL VOID RATIO	0.45	FINAL VOID RATIO	0.38
ESTIMATED SPECIFIC GRAVITY	2.540	SATURATED AT	95.785 KPa





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

SAMPLE SOURCE: N614 B-1@ 1.68 m - 1.98 m

SAMPLE PREP:

Undisturbed Saturate at 96 Kpa JOB NO:

1720134030.0002

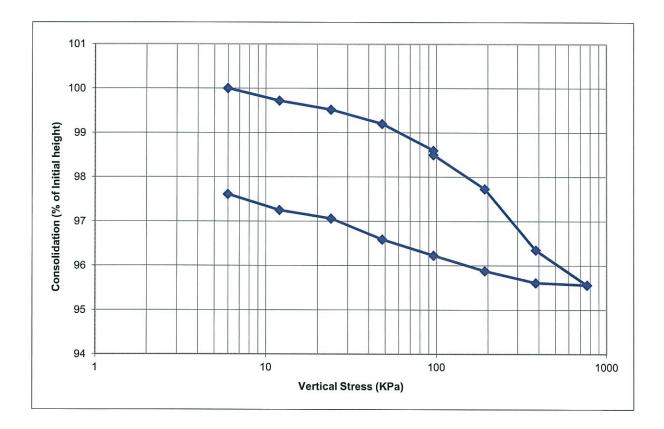
LAB NO:

WORK ORDER NO: 4 459

DATE SAMPLED: 11/4/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.37	FINAL VOLUME (cu.cm)	72.03
INITIAL MOISTURE CONTENT	12.0%	FINAL MOISTURE CONTENT	13.5%
INITIAL DRY DENSITY (kg per cu.m)	1900.8	FINAL DRY DENSITY (kg per cu.m)	1981.6
INITIAL DEGREE OF SATURATION	77%	FINAL DEGREE OF SATURATION	100%
INITIAL VOID RATIO	0.43	FINAL VOID RATIO	0.37
ESTIMATED SPECIFIC GRAVITY	2.710	SATURATED AT	95.785 KPa





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BIA project N12(12-2)(19-2)2+4

LOCATION:

Navajo, NM to N64 junction AZ (near Tsaile, AZ)

MATERIAL:

Bore hole samples

**SAMPLE SOURCE:** N614 B-2@ 4.57 m - 4.88 m

SAMPLE PREP:

Undisturbed

Saturate at 191 Kpa

JOB NO:

1720134030.0002

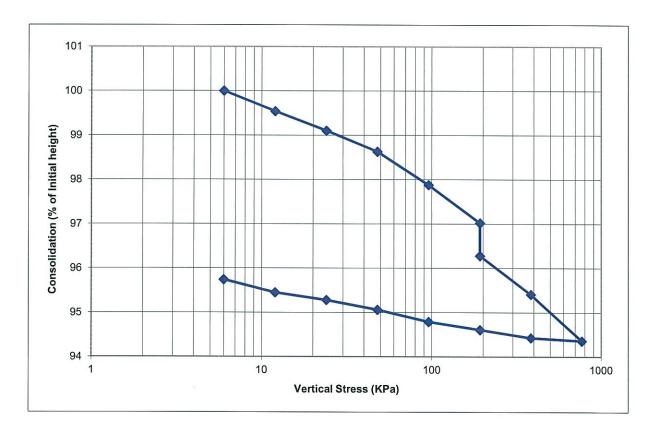
LAB NO:

WORK ORDER NO: 4 461

DATE SAMPLED: 11/4/13

### ONE-DIMENSIONAL CONSOLIDATION PROPERTIES OF SOILS (AASHTO T216-07)

INITIAL VOLUME (cu.cm)	75.37	FINAL VOLUME (cu.cm)	71.12
INITIAL MOISTURE CONTENT	15.5%	FINAL MOISTURE CONTENT	13.8%
INITIAL DRY DENSITY (kg per cu.m)	1818.8	FINAL DRY DENSITY (kg per cu.m)	1920.3
INITIAL DEGREE OF SATURATION	93%	FINAL DEGREE OF SATURATION	100%
INITIAL VOID RATIO	0.44	FINAL VOID RATIO	0.36
ESTIMATED SPECIFIC GRAVITY	2.610	SATURATED AT	191.57 KPa





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